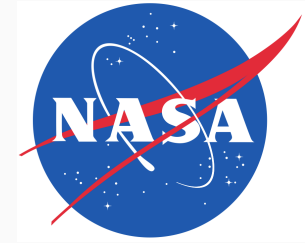


# Multimode detectors for cosmic microwave background studies

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The Second B-Mode from Space Workshop

December 05, 2017

Note: I am not Peter!

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<sup>3</sup>CRESST

# Outline

1. Introduction
2. Multimode bolometers for PIXIE
3. Multimode bolometers for sub-orbital applications
4. Conclusions

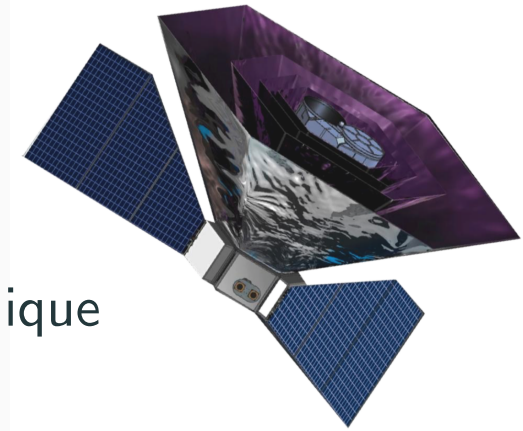
# Introduction

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# Introduction - the PIXIE experiment

The Primordial Inflation Explorer (PIXIE)

- Space-based polarizing Fourier transform spectrometer (FTS).



Detectors designed for a FTS like PIXIE require unique optimization:

- Large etendue ( $A\Omega = 4 \text{ cm}^2 \text{ sr}$ ).
- Handle large and constant optical load (120 pW).
- Large and mechanically robust absorber structure (30x larger than the spider web bolometers on Planck).
- Limited sensitivity to particle hits.
- Sensitive to all optical frequencies of interest (30 GHz - 6 THz).
- Photon-noise limited ( $\text{NEP}_{\text{phot}} \simeq 2.7 \times 10^{-16} \text{ W}/\sqrt{\text{Hz}}$ ).

Key difference: 4 multimoded bolometers instead of thousands of single moded bolometers.

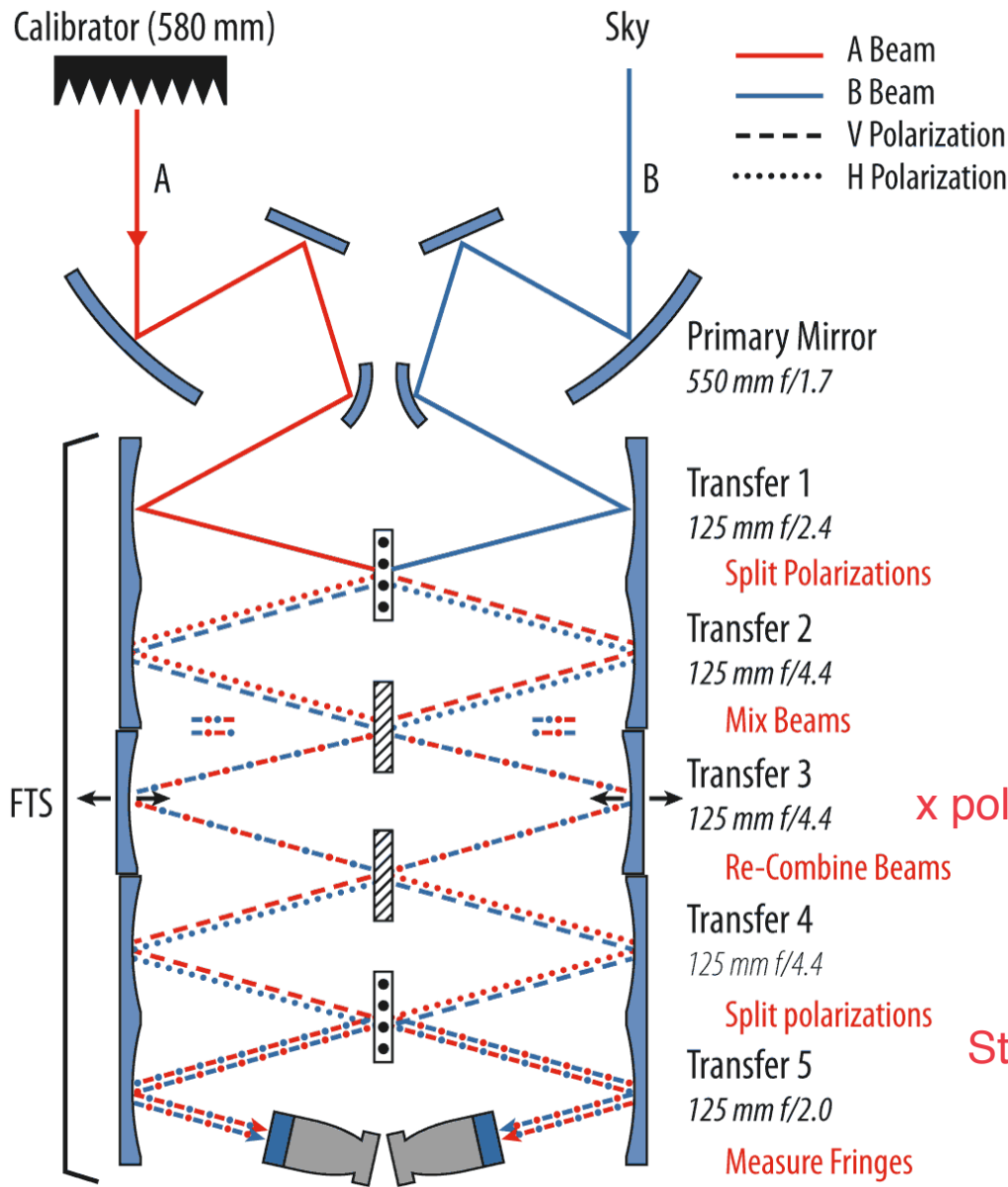
$$\text{NEP}_{\text{phot}} \propto A \times \Omega.$$

Photon noise equivalent power

Detector area

Solid angle

# Introduction - Fourier transform spectroscopy



Instrument computes the Fourier transform.

Incident light:

$$\mathbf{E}_{left} = A_x \hat{x} + A_y \hat{y}.$$

$$\mathbf{E}_{right} = B_x \hat{x} + B_y \hat{y}.$$

Power at detectors:

$$P = \frac{1}{2} \int (A_x^2 + B_y^2) + (A_x^2 - B_y^2) \cos\left(\frac{4\nu z}{c}\right) d\nu.$$

Difference spectrum

Inverse Fourier transform:

$$S_x^L(\nu) = A_x^2(\nu) - B_y^2(\nu).$$

x polarization from left

Mirror modulation

Sky-fixed coordinates:

y polarization from right

$$S_x^L(\nu) = Q_{sky} \cos(2\gamma) + U_{sky} \sin(2\gamma).$$

Stokes Q

Spacecraft spin angle

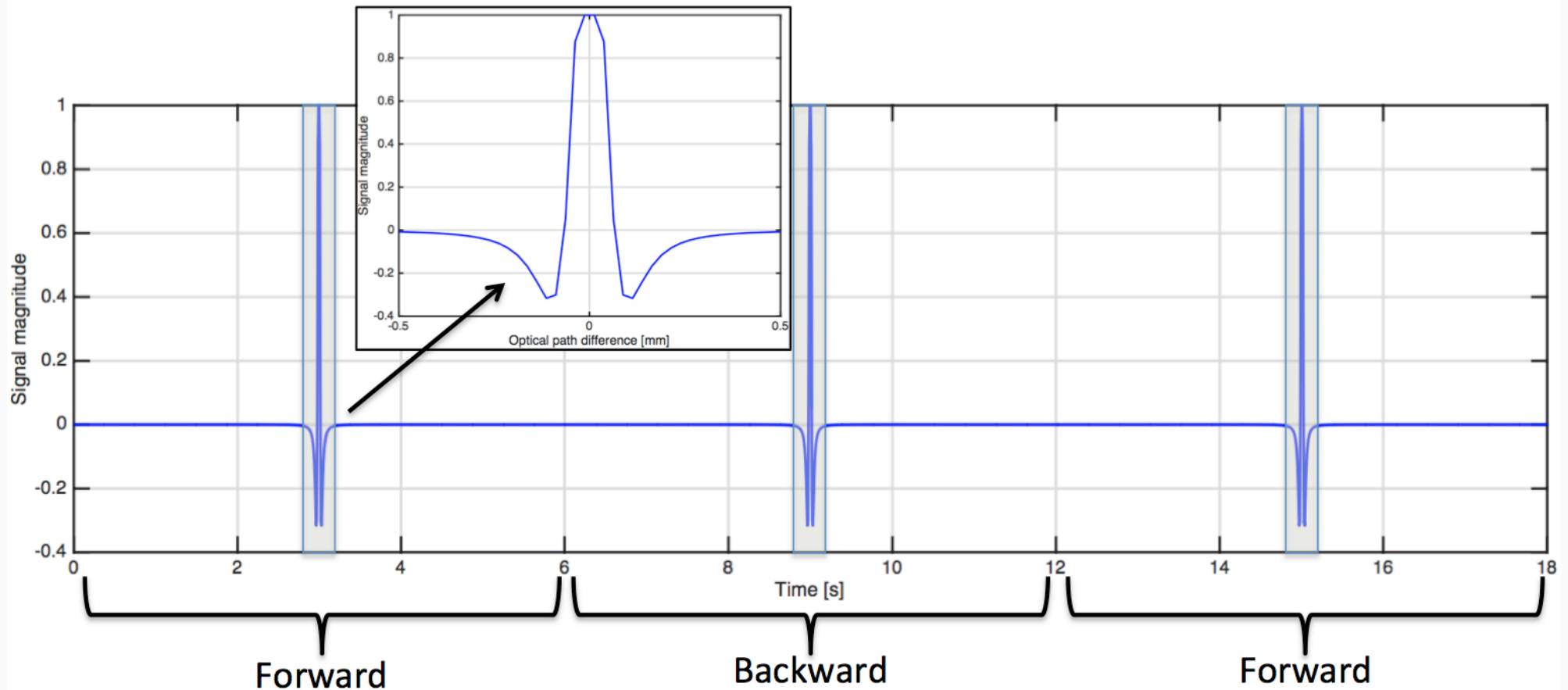
Stokes U

Completely specifies linear polarization.

Using a FTS is the *ideal* way to measure polarization.

# Introduction - Fourier transform spectroscopy

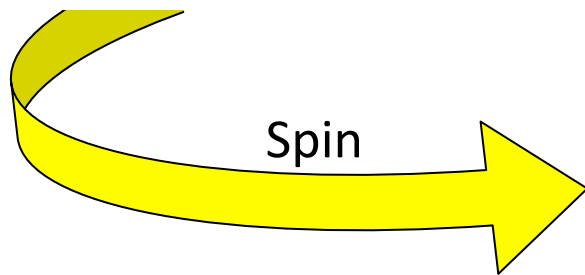
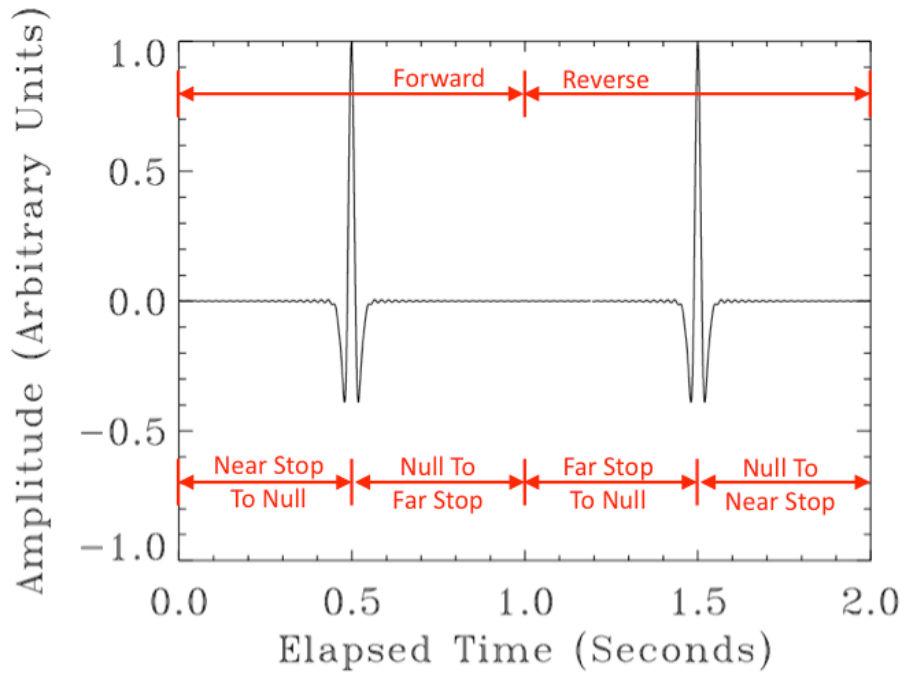
Signal is the Fourier transform of the sky. What does it look like?



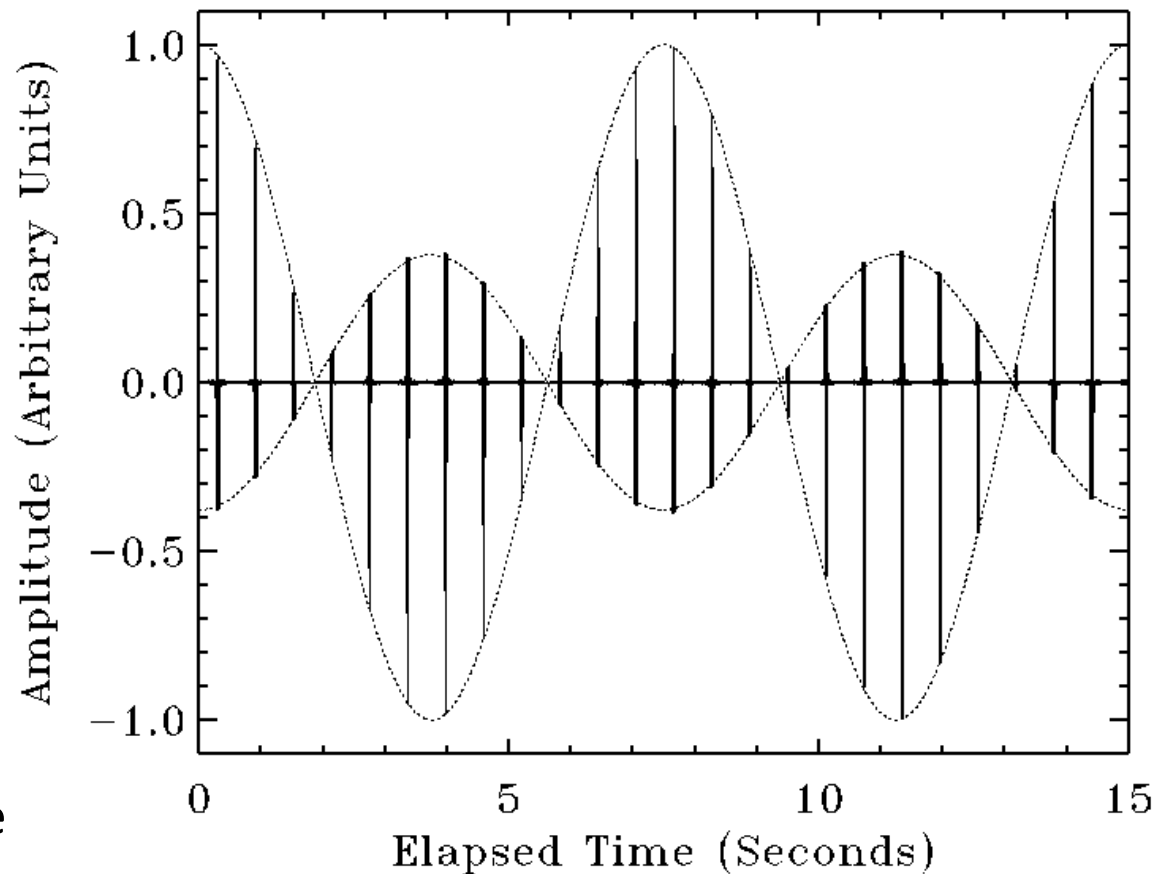
**Details of FTS operation give bolometer bias and bandwidth requirements.**

For PIXIE: photon noise limited ( $\text{NEP}_{\text{phot}} \simeq 2.7 \times 10^{-16} \text{ W}/\sqrt{\text{Hz}}$ ) across all FTS frequencies (0 – 100 Hz) under large, near-constant ( $\sim 120 \text{ pW}$ ) optical bias.

# Introduction - Fourier transform spectroscopy



Spacecraft rotation creates ***amplitude modulation*** of polarization fringe pattern



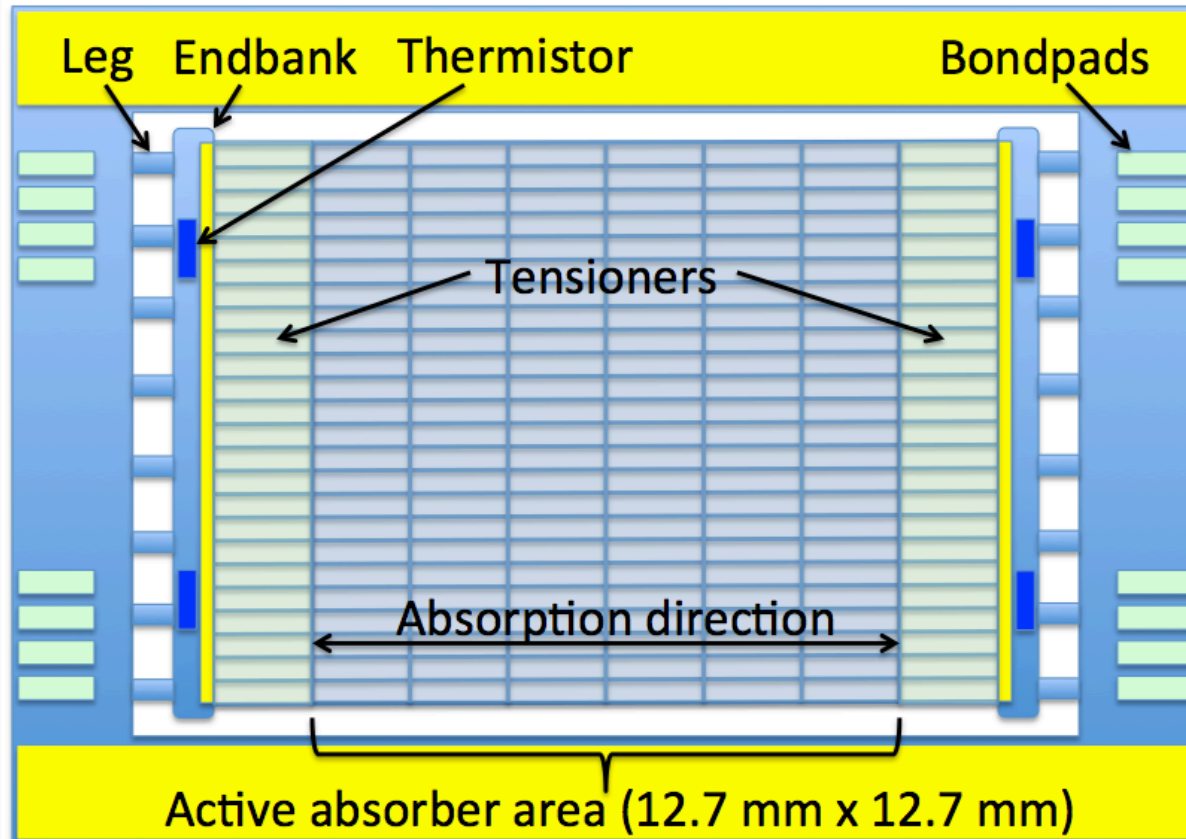
Instrumental drifts in time domain are Fourier transformed to lowest bins in frequency domain  
***No striping in polarization sky maps***

# Multimode bolometers for PIXIE

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# PIXIE bolometers - Introduction

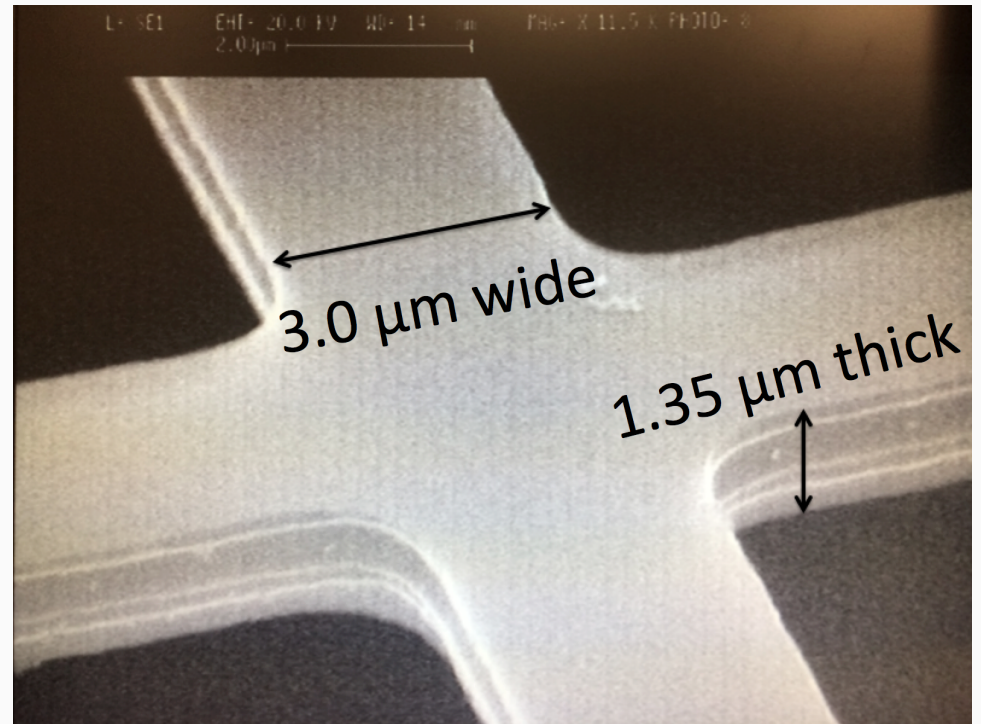
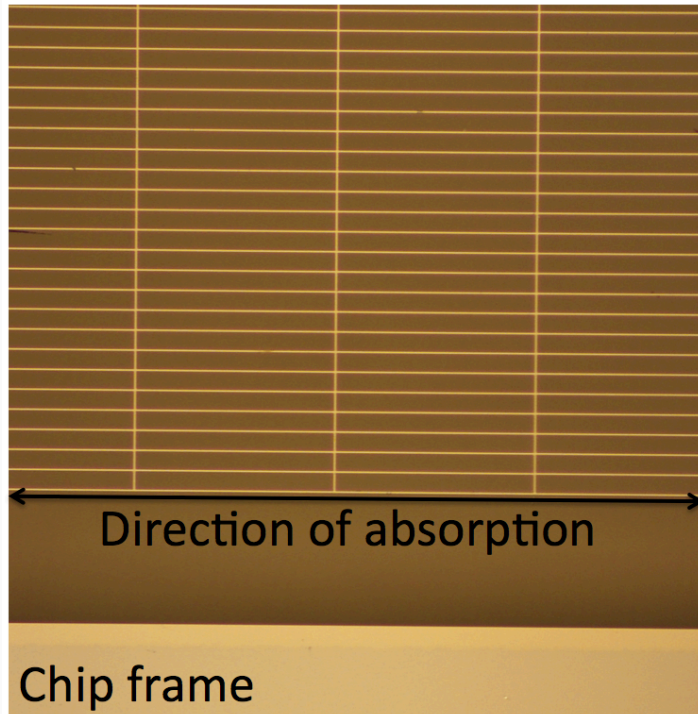


Key components:

- Absorber structure - absorb single linear polarization
- Endbanks - measure incident optical power with silicon thermistors
- Frame - thermal sink, indium bumps, and interface to readout

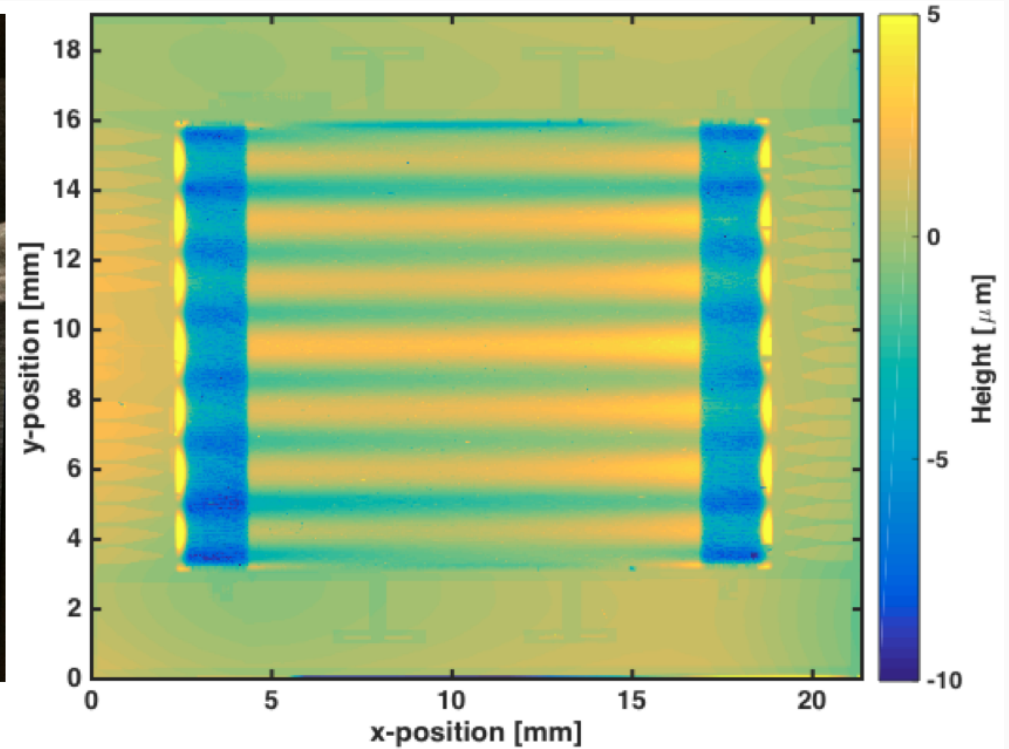
Single-crystal silicon instead of SiN to control time constants  
Gold plate frame to eliminate back-loading from cosmic ray hits

# PIXIE bolometers - Absorber structure



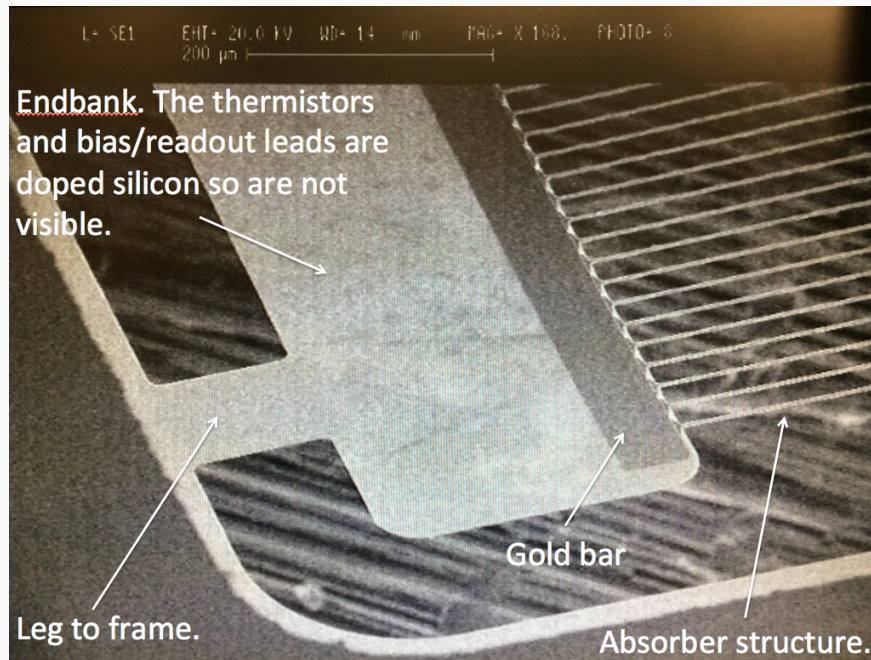
- Grid of degenerately-doped Si wires.
- Metallic at all temperatures;  $R_s^{eff} \sim 377 \Omega/\square$ .
- Absorber area  $A$  sets low frequency cutoff of instrument ( $\sim 15$  GHz); grid spacing ( $30 \mu\text{m}$ ) sets high frequency cutoff ( $\sim 5$  THz).
- Wire widths and thicknesses are highly uniform across the array.
  - Thickness set by starting SOI device layer thickness ( $1.35 \mu\text{m}$ ).
  - Wires are etched to width with an ICP RIE process.

# PIXIE bolometers - Absorber structure



- Doping induces compressive stress in absorber wires.
- Detectors subject to vibrations and acoustic excitations at launch.
- Solution: deposit highly tensile  $\text{Al}_2\text{O}_3$  film on absorbers outside of active optical region.
  - Fabricated absorbers are flat and expected to oscillate with amplitudes of  $< 0.4 \mu\text{m}$  rms during launch.

# PIXIE bolometers - Endbanks



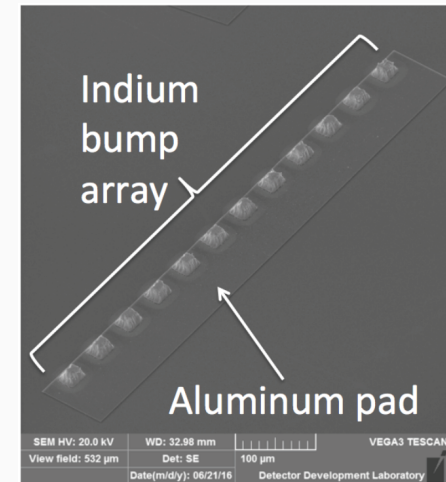
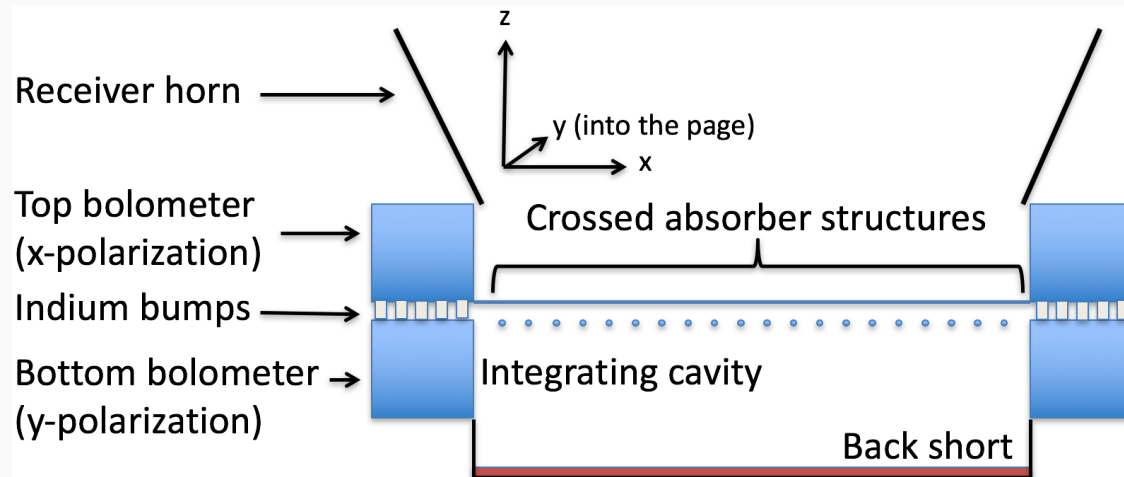
- Consists of a gold bar for thermalization and two doped silicon thermistors on a crystalline silicon membrane.
  - The gold bar also sets the heat capacity of the endbank.
  - Endbank is formed from the device layer of the SOI substrate.
- Endbanks are connected to the chip frame through eight silicon legs.
  - Thermistors are doped to operate below metal-insulator transition. Electron transport mechanism is variable range hopping:

$$R(T) = R_0 \times \exp \sqrt{\frac{T_0}{T}},$$

where  $R_0$  and  $T_0$  are constants largely determined by geometry and doping, respectively.

# PIXIE bolometers - Chip frame

Focal plane: two In bump-hybridized detectors mounted  $< 20 \mu\text{m}$  apart with their absorbers orthogonal.

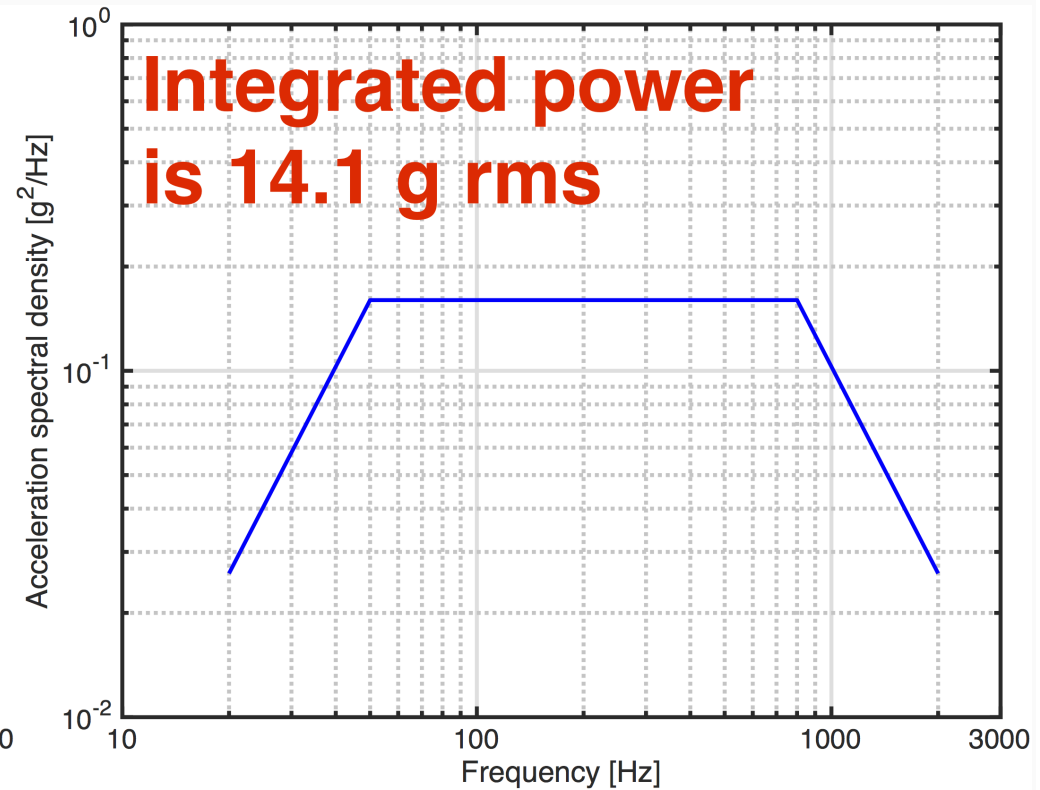
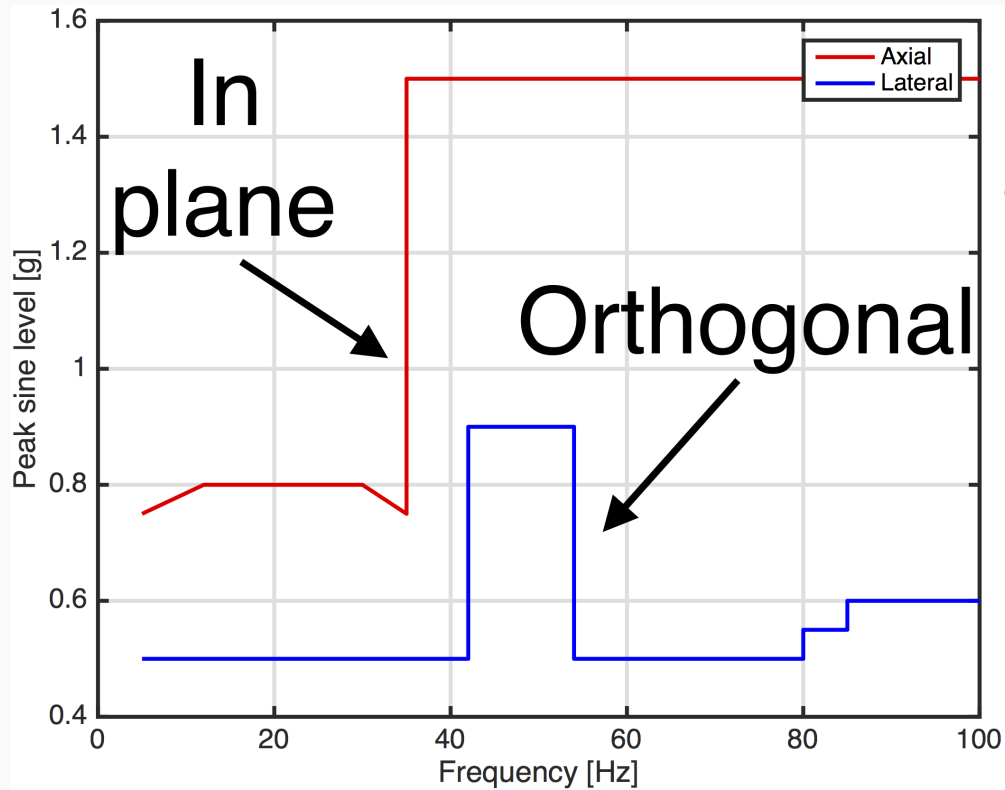


- Any two bolometer chips can be hybridized together.
- Large gold-covered areas serve as heat sinks.
- Al pads alloyed to degenerately-doped Si leads form wirebond and In bump pads.

Prototypes: achieved chip separation of  $13 \pm 1 \mu\text{m}$ .



# PIXIE bolometers - Environmental tests

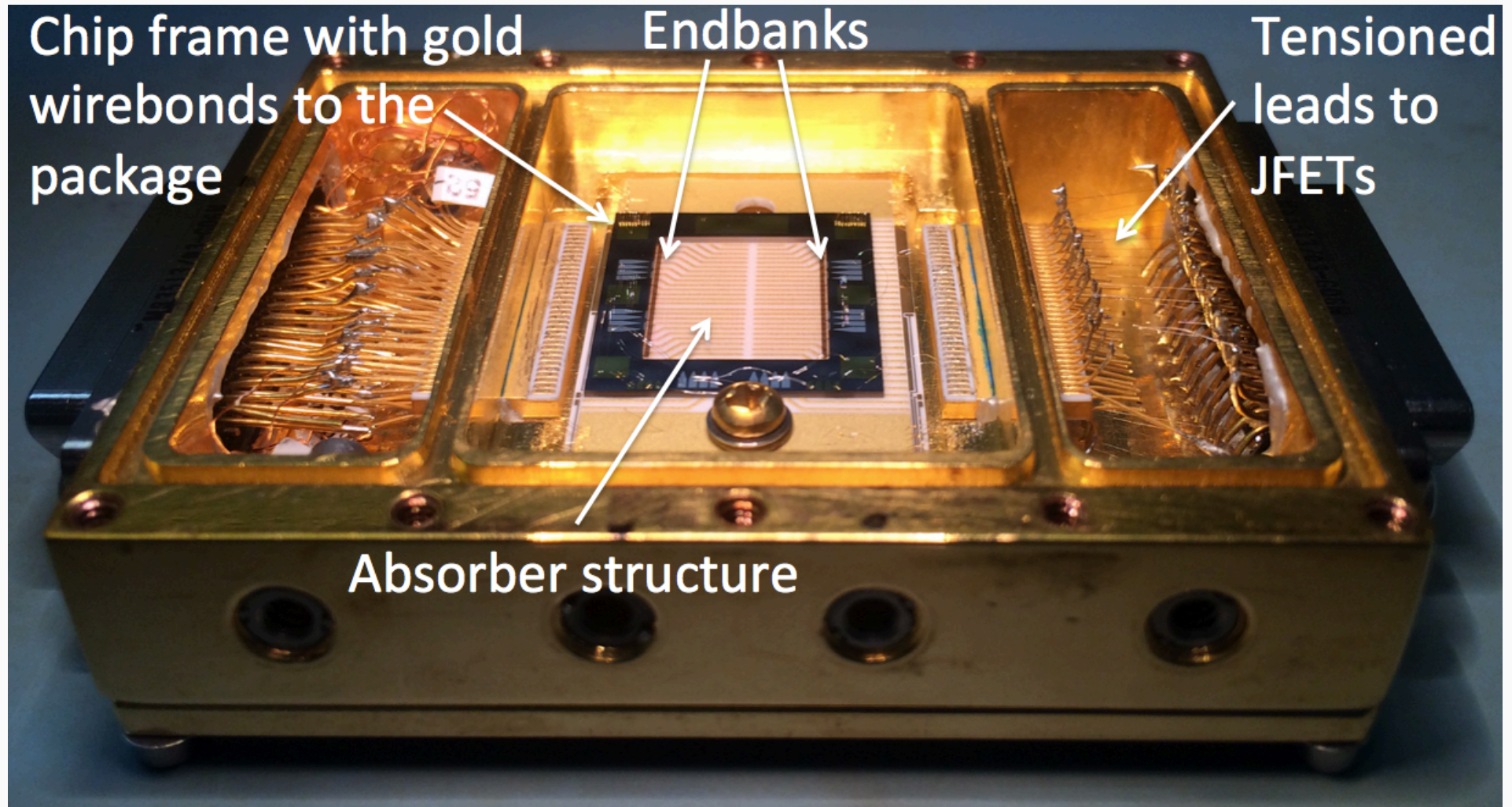


# PIXIE bolometers - Environmental tests



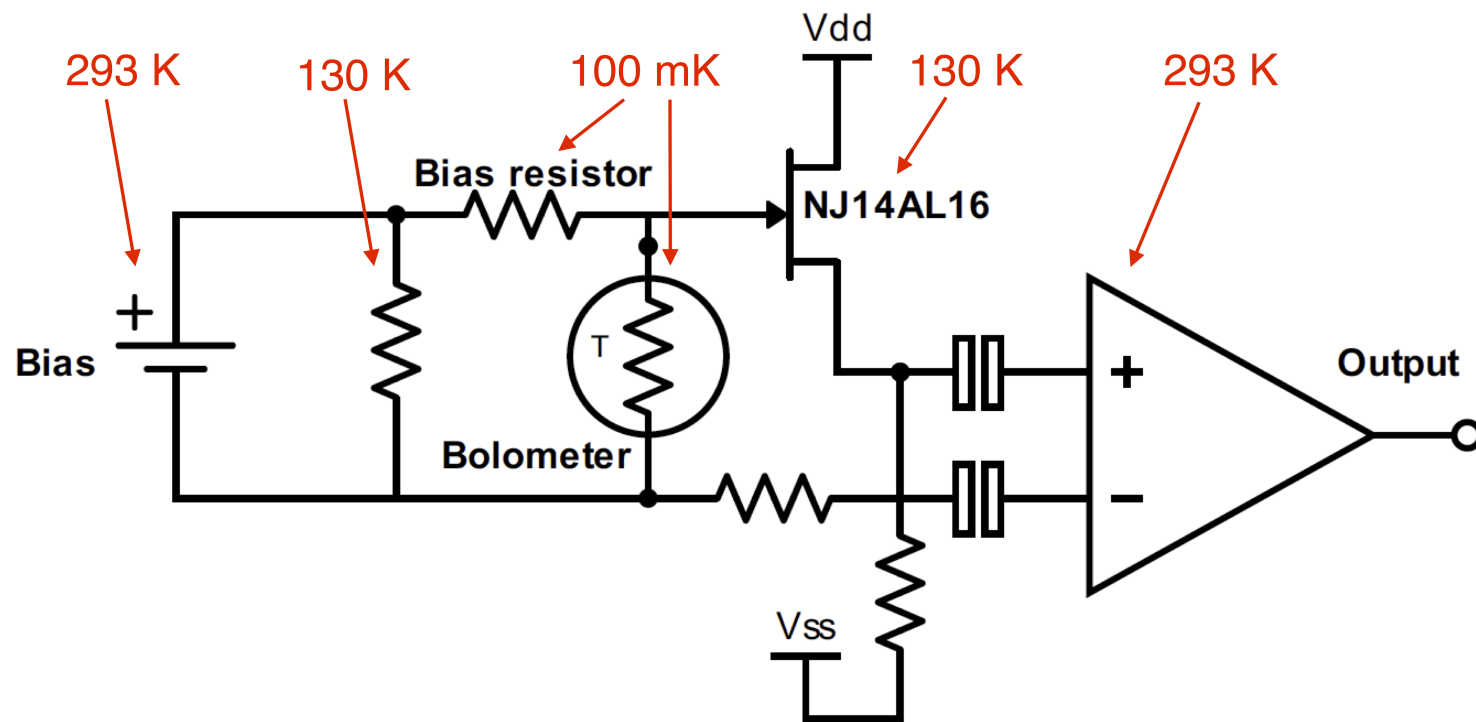


# PIXIE bolometers - Cryogenic test package



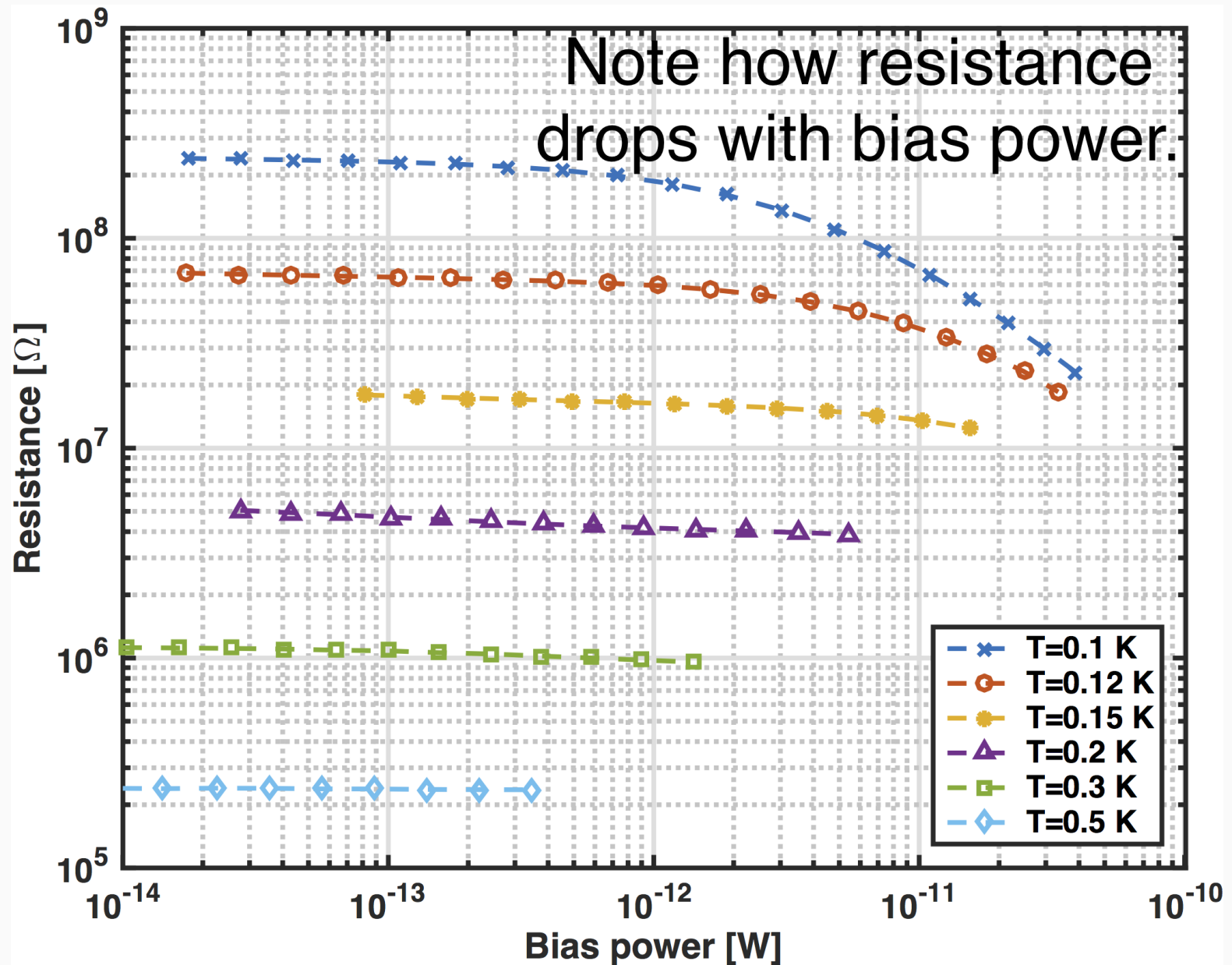
- Bolometer is connected to a cryogenic (130 K) JFET amplifier with tensioned leads, mitigating capacitive microphonic contamination of the signal band. **Shamelessly borrowed from Hitomi.**

# PIXIE bolometers - Readout circuit



- Thermistor operates under current bias ( $R_{bias} \gg R_{therm}$ ).
- We use Interfet NJ14AL16 JFETs that are screened for low noise performance at 130 K ( $5.5 \text{ nV}/\sqrt{\text{Hz}}$  at 100 Hz).
- Amplifier converts the high source impedance of the thermistors ( $\text{M}\Omega$ -scale) to the low output impedance of the JFETs ( $1.8 \text{ k}\Omega$ ).
- Low impedance signal is AC coupled to a room temperature amplifier.

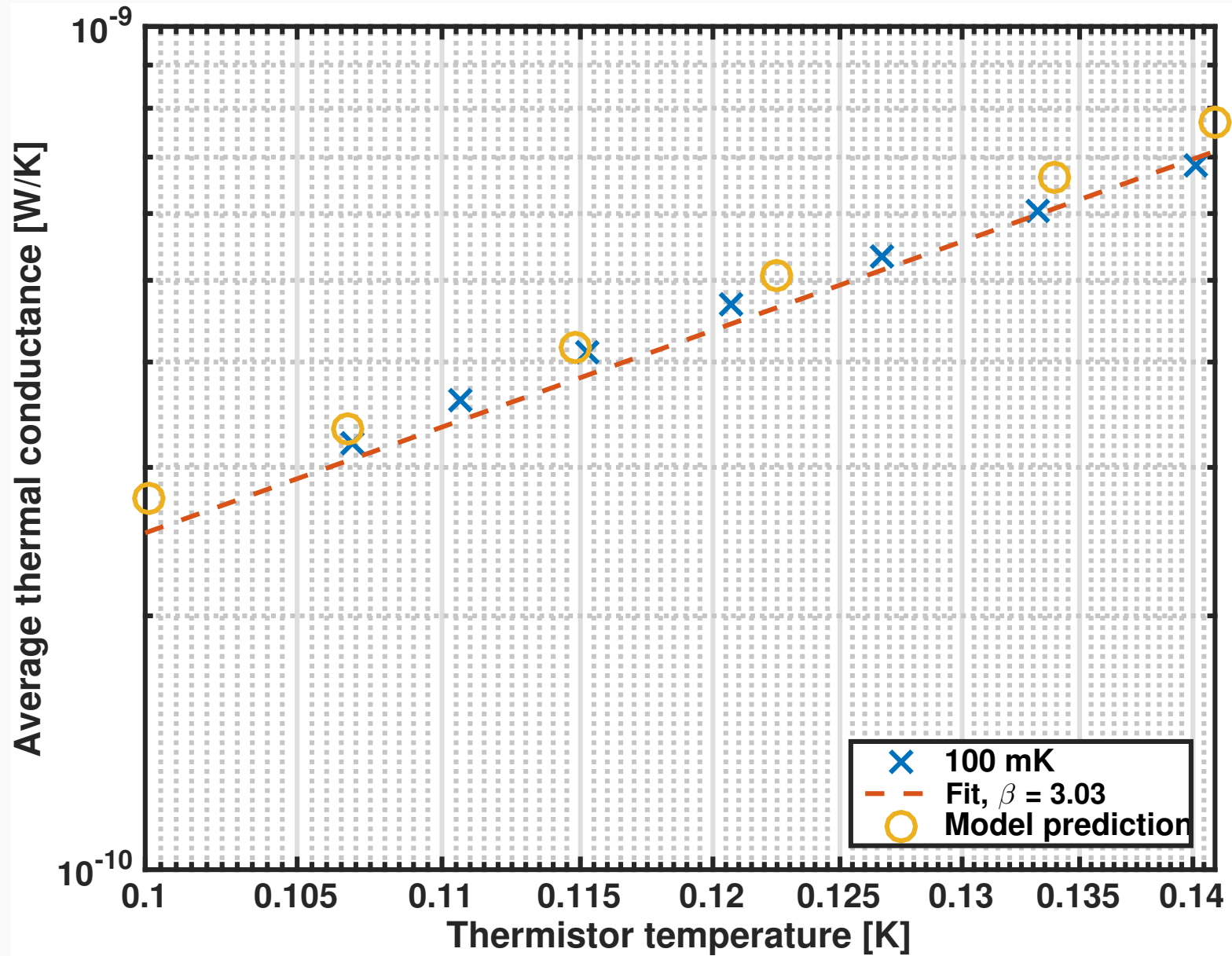
# PIXIE bolometers - Load curves



$T_0 = 15.11$  K.  $R_0 = 911$  Ω. Operating resistance: 5.42 MΩ.

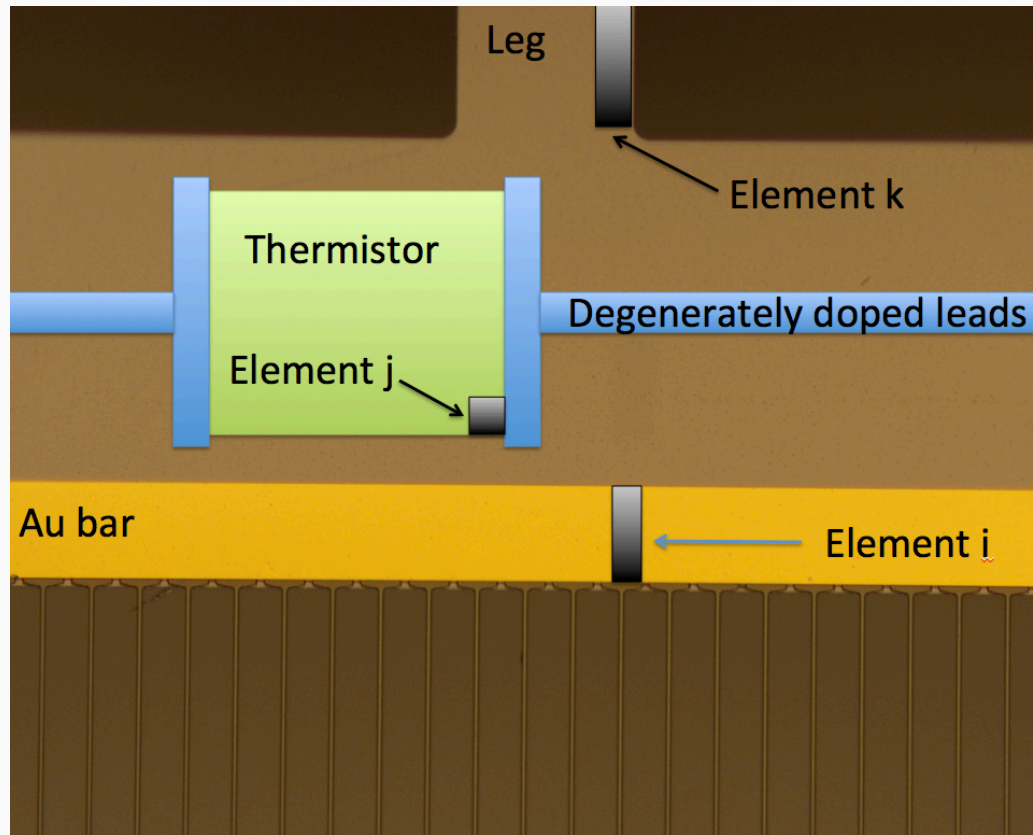
Old school detectors: Robust vs loading (but hard to multiplex)

# PIXIE bolometers - Thermal conductance



- $\bar{G} = P_{\text{bias}} / (T_1 - T_2)$ ; fit with function  $\tilde{G} = G_0 \times T^\beta$ .

# PIXIE bolometers - Thermal model

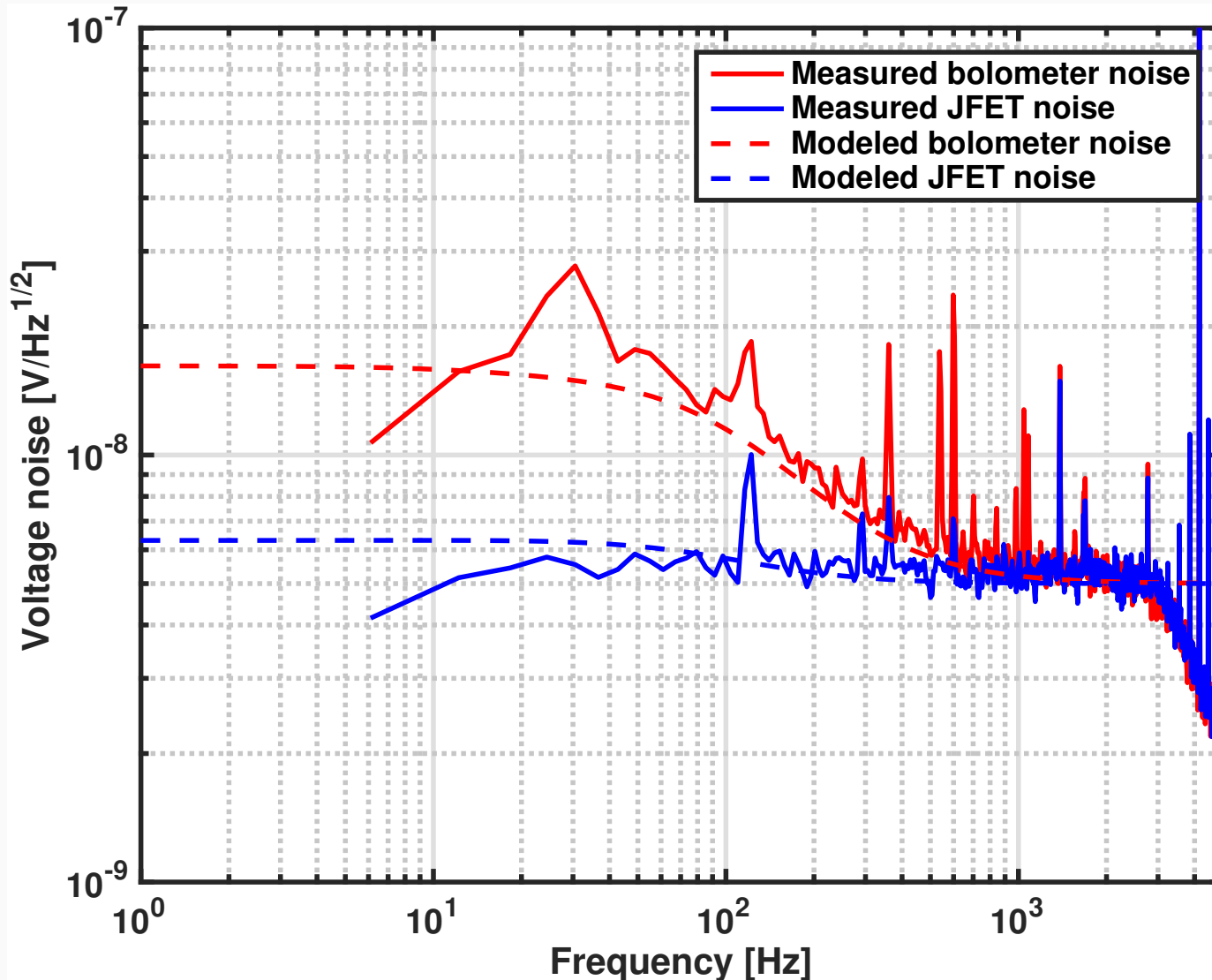


Solve for non-equilibrium bolometer noise:

$$\text{NEP}_{\text{bolometer}}^2 = \gamma_1 4k_b T^2 G + \frac{1}{S^2} \left( \gamma_2 4k_b TR + e_n^2 + \gamma_3 i_n^2 R + \gamma_4 \text{NEP}_{\text{excess}}^2 \right).$$

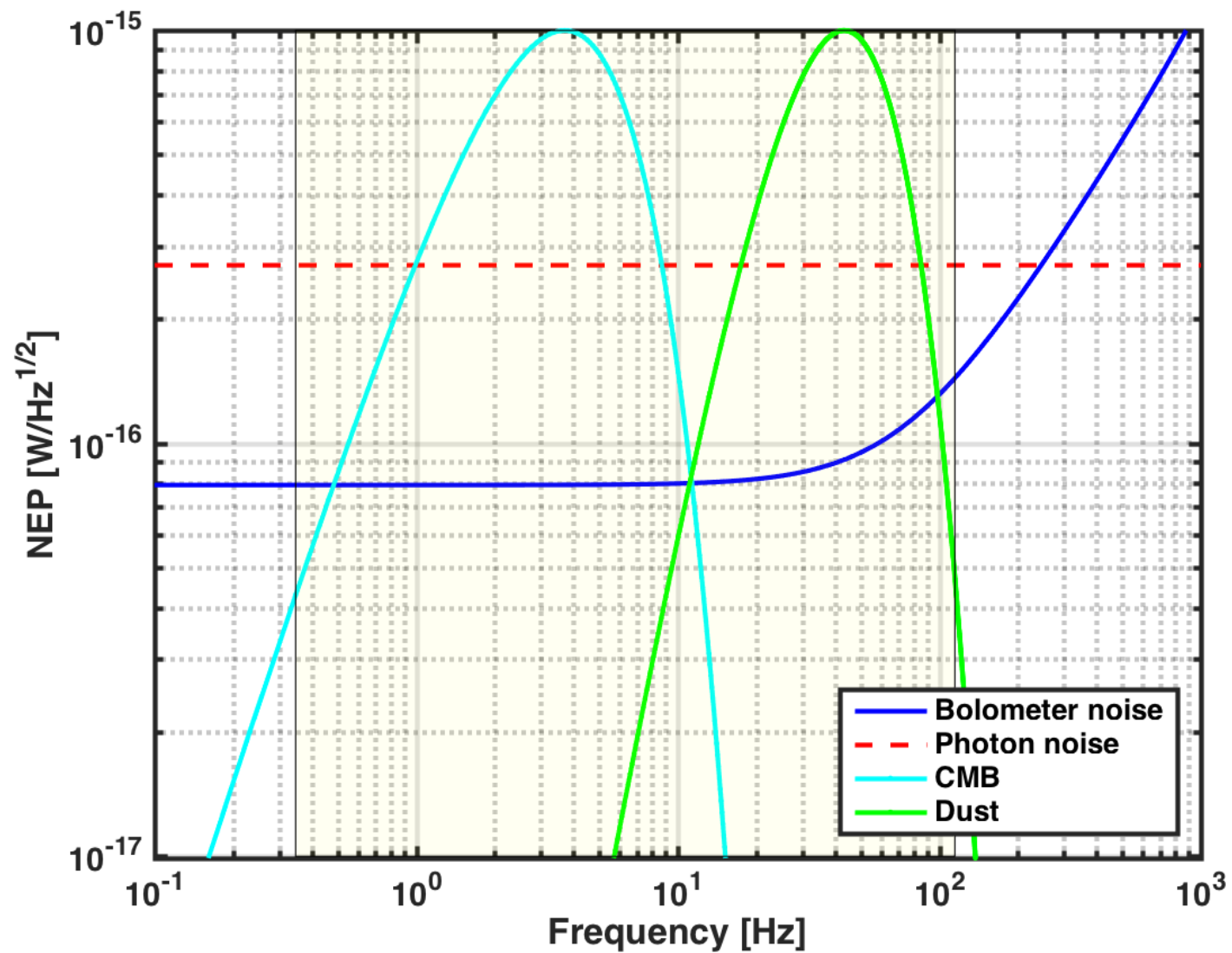
Total NEP      Phonon noise      Responsivity      Johnson noise      Amplifier noise      Excess noise

# PIXIE bolometers - Noise



- Modeled noise fits the measured noise well for multiple bias conditions.

# PIXIE bolometers - Noise



*Expect to be photon noise limited across the entire PIXIE bandwidth.*

# **Multimode bolometers for sub-orbital applications**

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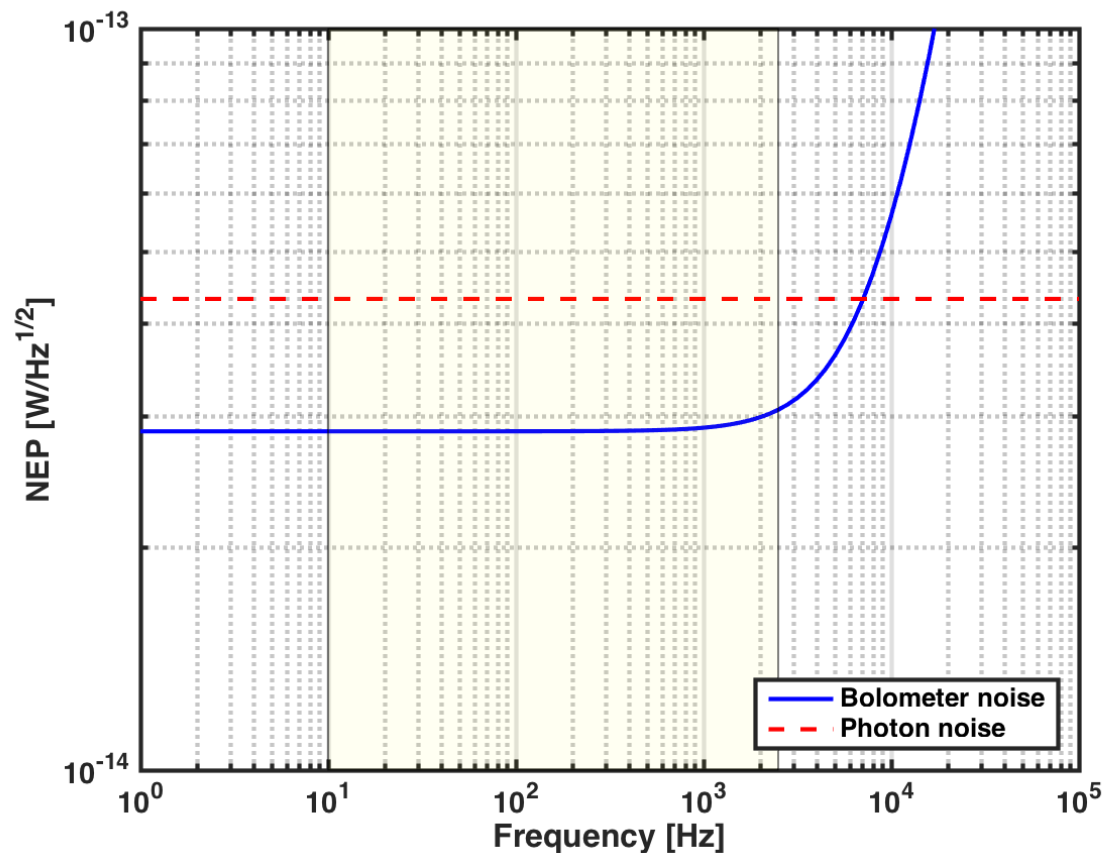


# Bolometers for Dust Buster

Thermistor-based bolometers can operate over a wide temperature and load range. Preliminary sensitivity for Dust Buster-like operating conditions:

- $\nu_{max} = 2.5$  THz.
- $P_{optical} = 1.2 \mu\text{W}$ .
- $T_{bath} = 0.3$  K.

Balloon mission to measure dust SED  
along individual lines of sight  
over frequency range 100 GHz — 2.5 THz



# Conclusions

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# Conclusions

We designed, built, and tested detectors suitable for a space-based FTS like PIXIE

- Optimization is different from single-mode bolometers.
- Fabrication process is high-yield and detectors are mechanically robust.
- Readout system is mature and well-understood.
- Cryogenic testing indicates performance meets requirements for a PIXIE-like instrument.

Thermistor-based bolometers are tolerant of wide operating conditions

- Minimal changes are needed to make a multimode bolometer suitable for a sub-orbital FTS.

# Acknowledgements

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Special thanks to all who contributed to this development effort.

**Questions?**