

Bubble wall velocities in local thermal equilibrium

2109.13710

1. Motivations

SM is not complete:

- Dark Matter
- Matter-anti-matter asymmetry
- Inflation
- Strong CP problem, see, however, 2001.07152

Detection of new physics:

- Energy frontier
- Intensity frontier
- Cosmic frontier : GWs PT strength

GWs from 1st PTs : H_* , α , V_w , β ← transition rate
 ↑
 Hubble parameter during percolation

2. Total force on a bubble wall

Coupled system

Scalar field ϕ + plasma $f_i(p, x)$

$$\text{EOM: } \square\phi + \frac{\partial V(\phi)}{\partial\phi} + \sum_i \frac{dm_i^2(\phi)}{d\phi} \int \frac{d^3\vec{p}}{(2\pi)^3 2E_i} f_i(p, x) = 0, \quad \frac{df_i}{dt} = -C[f_i]$$

Can be derived more systematically from the 2PI effective action

$$\frac{\delta \Gamma_{2PI}[\phi, \Delta_i]}{\delta\phi} = 0, \quad \frac{\delta \Gamma_{2PI}[\phi, \Delta_i]}{\delta\Delta_i} = 0$$

imaginary time → Gap equation
 in some limit/approximation

$$\Gamma_{2pI}[\phi, \Delta\phi, \dots] = S[\phi] + \frac{i}{2} \text{Tr} \ln(\Delta\phi^{-1}) + \frac{i}{2} \text{Tr}(G_{\phi\phi} \Delta\phi) + \dots$$

eg: $\left(\frac{i}{2} \text{Tr} \ln(\Delta\chi^{-1}) + \frac{i}{2} \text{Tr}(G_{\chi\chi}(\phi) \Delta\chi) \right)$

Taking $f_i(p, x) = f_i^{\text{eq}}(p, x) + \delta f_i(p, x)$

$$\Rightarrow \square\phi + \frac{\partial V_{\text{eff}}(\phi, T)}{\partial\phi} + \sum_i \frac{dm_i^2(\phi)}{d\phi} \int \frac{d^3\vec{p}}{(2\pi)^3 2E_i} \delta f_i(p, x) = 0$$

(equilibrium) (out-of-equilibrium)

↳ dissipative friction

Conventional understanding: finite v_w require nonvanishing dissipative friction

not true!

$$\int dz \frac{d\phi}{dz} \left(\square\phi + \frac{\partial V_{\text{eff}}(\phi, T)}{\partial\phi} + \sum_i \frac{dm_i^2(\phi)}{d\phi} \int \frac{d^3\vec{p}}{(2\pi)^3 2E_i} \delta f_i(p, x) \right) = 0$$

$$\begin{aligned} \int dz \frac{d\phi}{dz} \frac{\partial V_{\text{eff}}(\phi, T)}{\partial\phi} &= \int dz \left(\frac{dV_{\text{eff}}}{dz} - \frac{\partial V_{\text{eff}}}{\partial T} \frac{dT}{dz} \right) \\ &= \Delta V_{\text{eff}} - \int dz \frac{\partial V_{\text{eff}}}{\partial T} \frac{dT}{dz} \end{aligned}$$

$$\Rightarrow \Delta V_{\text{eff}} = \int dz \frac{\partial V_{\text{eff}}}{\partial T} \frac{dT}{dz} - \sum_i \int dz \frac{d\phi}{dz} \frac{dm_i^2(\phi)}{d\phi} \int \frac{d^3\vec{p}}{(2\pi)^3 2E_i} \delta f_i(p, x) = 0$$

↑ driving force backreaction force

$$= \frac{F_{\text{back}}}{A}$$

Thermal equilibrium: $\frac{F_{\text{back}}}{A}$ not necessarily vanish!

Condition: $\frac{dT}{dz} \neq 0$

Dissipative friction force

→ runaway

• Leading order v_w -independent 0903.4099

• Higher-order v_w -dependent → subluminal speeds

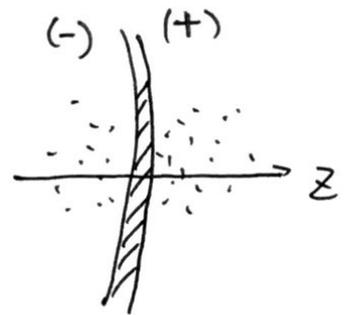
1703.08215, 2007.10343 (Yi-Kun's talk)

3. "Friction" in local thermal equilibrium & a new matching condition.

Energy-momentum conservation:

$$\bar{T}_\phi^{\mu\nu} = (\partial^\mu \phi)(\partial^\nu \phi) - g^{\mu\nu} \left(\frac{1}{2} (\partial\phi)^2 - V(\phi) \right)$$

$$\bar{T}_f^{\mu\nu} = (\rho_f + p_f) u^\mu u^\nu - p_f g^{\mu\nu}$$



$$\bar{\nabla}_\mu \bar{T}^{\mu 0} = 0 \Rightarrow \omega \gamma^2 v = \text{const}$$

$$\bar{\nabla}_\mu \bar{T}^{\mu 3} = 0 \Rightarrow \omega \gamma^2 v^2 + \frac{1}{2} (\partial_z \phi(z))^2 + p = \text{const}$$

Here $\rho = \rho_f - V(\phi)$, $p = \rho_f + V(\phi)$, and $\omega = \rho_f + p_f = \rho + p$
 ↑
 enthalpy

Well-known matching conditions:

$$\omega_+ \gamma_+^2 v_+ = \omega_- \gamma_-^2 v_-$$

$$\omega_+ \gamma_+^2 v_+^2 + p_+ = \omega_- \gamma_-^2 v_-^2 + p_-$$

recall
 $\omega = Ts$
 $\gamma^2 v^2 = \gamma^2 - 1$

$$p_- - p_+ = A \{ (\gamma^2 - 1) Ts \}$$

$$\Rightarrow \frac{F_{\text{pressure}}}{A} \equiv \Delta V_{\text{eff}}, \quad \frac{F_{\text{back}}}{A} = \Delta \{ (\gamma^2 - 1) Ts \}$$

(thermal equilibrium)

in general: $p_- - p_+ = \Delta V_{\text{eff}} - \Delta S p_f$ out-of-equilibrium effects

Recently, 2005.10875 proposed

$$\frac{F_{\text{back}}}{A} = (\gamma_w^2 - 1) T \Delta S \rightarrow \text{not correct}$$

because they assumed
constant temperature
across the wall!

Entropy conservation:

$$\partial_\mu S^\mu \equiv \partial_\mu (S U^\mu) = 0 \Rightarrow$$

$$\left. \begin{aligned} S(z) \gamma(z) v(z) &= \text{const} \\ \gamma^2 - 1 &= \gamma^2 v^2 \end{aligned} \right\}$$

Further

$$\left\{ \begin{aligned} w = T S \\ w \gamma^2 v &= \text{const} \\ S(z) \gamma(z) v(z) &= \text{const} \end{aligned} \right.$$

$$\Rightarrow \frac{F_{\text{back}}}{A} = \text{const} \times A \{ \gamma v T \}$$

$$\Rightarrow \gamma(z) T(z) = \text{const}$$

New matching condition for

local equilibrium $\boxed{\gamma_+ T_+ = \gamma_- T_-}$

4. Bubble velocities in local thermal equilibrium

Bag equation of state:

$$p = a T^4 + \epsilon$$

$$p = \frac{1}{3} a T^4 - \epsilon$$

Generalized: $a(T, \phi), \epsilon(T, \phi)$

Hydrodynamic quantities: $T(z), v(z) \Rightarrow (\gamma_+, T_-, v_+, v_-)$

related to T_{nuc} treated as
given

$$\omega_+ \gamma_+^2 v_+ = \omega_- \gamma_-^2 v_- \quad \text{--- (1)}$$

$$\omega_+ \gamma_+^2 v_+ + p_+ = \omega_- \gamma_-^2 v_- + p_- \quad \text{--- (2)}$$

$$\gamma_+ T_+ = \gamma_- T_- \quad \text{--- (3)}$$

Need assumption on $b \equiv \frac{a_-}{a_+}$ model-dependent

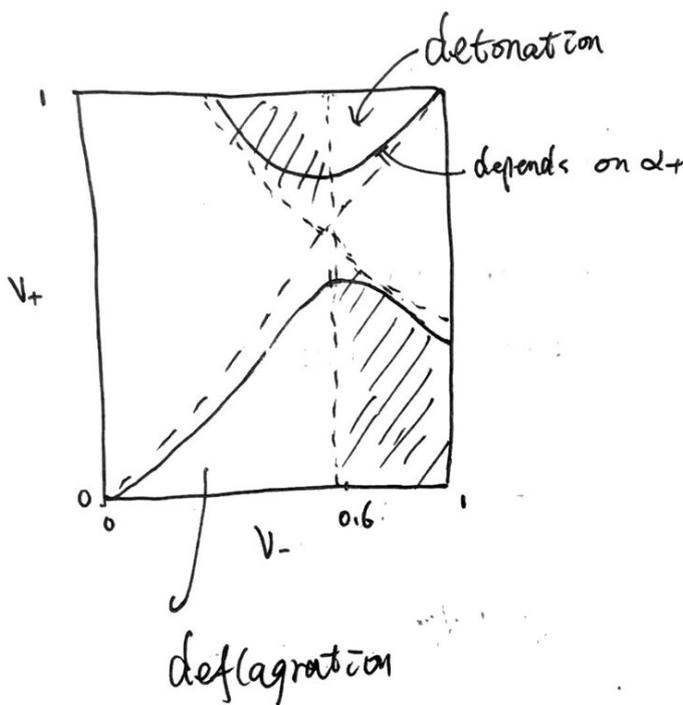
① & ②:

$$v_+ v_- = \frac{1 - (1 - 3\alpha_+) \gamma}{3 - 3(1 + \alpha_+) \gamma}$$

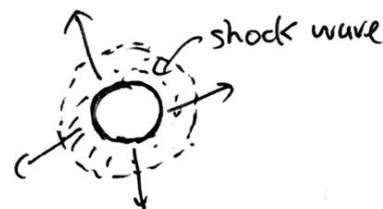
$$\frac{v_+}{v_-} = \frac{3 + (1 - 3\alpha_+) \gamma}{1 + 3(1 + \alpha_+) \gamma}$$

$$\alpha_+ \equiv \frac{\Delta E}{a_+ T_+^4}, \quad \gamma \equiv \frac{a_+ T_+^4}{a_- T_-^4}$$

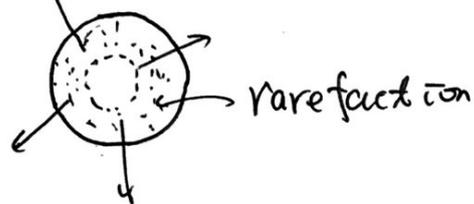
$$\Rightarrow v_+ = \frac{1}{6(1 + \alpha_+) v_-} \left[1 + 3v_-^2 \pm \sqrt{1 + 6(6\alpha_+^2 + 4\alpha_+ - 1)v_-^2 + 9v_-^4} \right]$$



deflagration $v_w < c_s$



detonation $v_w > c_s$



We can also obtain

$$v_- = \frac{1}{6v_+} \left[1 - 3\alpha_+ + 3(1 + \alpha_+)v_+^2 \pm \sqrt{[1 - 3\alpha_+ + 3(1 + \alpha_+)v_+^2]^2 - 12v_+^2} \right]$$

Detonations



$$v_+ = v_w$$

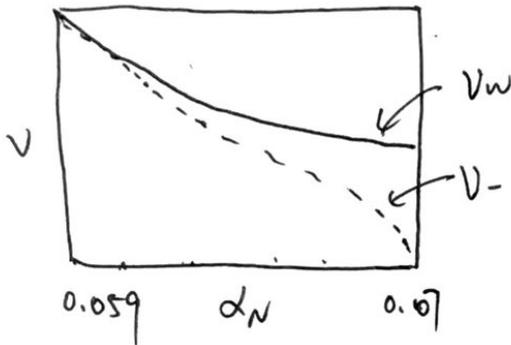
$$T_+ = T_{nuc}$$

$$\alpha_+ = \frac{\Delta E}{a(T_{nuc}) T_{nuc}^4} \equiv \alpha_N$$

From (2) & (3) $\left(\frac{\gamma_w}{\gamma_-}\right)^4 b + 3(1 + \alpha_N)$

$$\Rightarrow v_- = v_w \quad 3\left(\frac{\gamma_w}{\gamma_-}\right)^4 + (1 - 3\alpha_N)$$

$b \approx 0.85$ for SM



$$\Delta F = (p_- - p_+) |_{T_{nuc}}$$

$$= \frac{T_{nuc}^4}{3} (a_- - a_+) - (\epsilon_- - \epsilon_+) \geq 0$$

$$\Rightarrow \alpha_N \geq \frac{1-b}{3} = 0.05$$

$$[\alpha_{min} \approx 0.059, \alpha_{max} \approx 0.07]$$

Deflagrations:

$$v_- = v_w$$

Now we need to relate (T_+, α_+) to (T_{nuc}, α_N)

$$\alpha_+ = \frac{\Delta E}{\alpha_+ T_+^4} = \frac{\Delta E}{a_{nuc} T_{nuc}^4} \cdot \frac{a_{nuc} T_{nuc}^4}{a_+ T_+^4} \equiv \alpha_N \frac{g^4}{b}$$

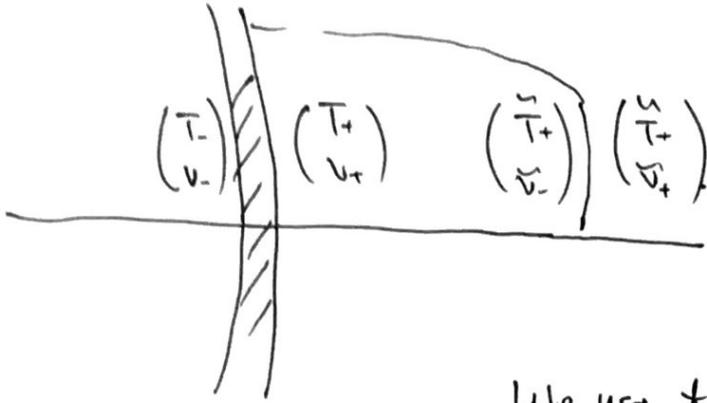
$$b = \frac{a_+}{a_{nuc}} \approx 1, \quad g = \frac{T_{nuc}}{T_+}$$



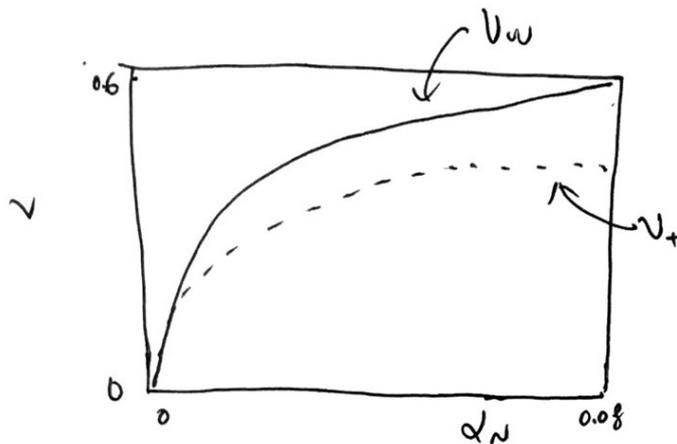
- need to solve the fluid velocity and temperature profile away from the bubble wall



$$\alpha_+ = 0$$



We use the planar-wall approximation
and the matching conditions
at the shock-wave front



$$[\alpha_{\min} \approx 0.0500061, \alpha_{\max} \approx 0.0789645]$$

Combining the analysis for detonations & deflagrations

\Rightarrow Steady state for $\alpha_N < \alpha_{\text{crit}} = \alpha_{\max}$

Run away for $\alpha_N > \alpha_{\text{crit}}$