

# SQUIDs for FDM

## in Satellite CMB Experiments

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B-modes From Space

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# SQUIDs for FDM

## in Satellite CMB Experiments

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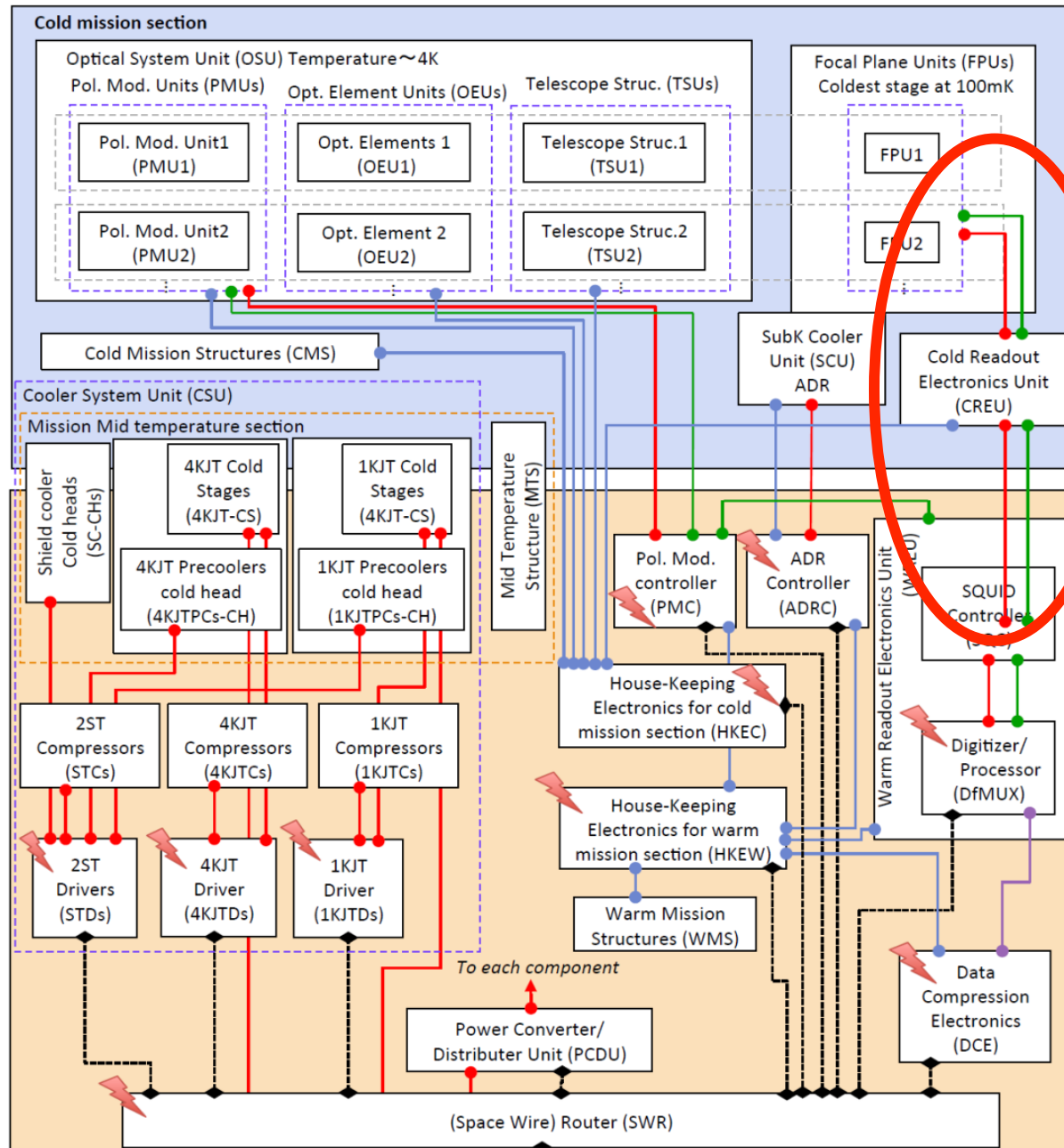
# SQUIDs for FDM in Satellite CMB Experiments

## Outline

- Scope of talk
- Context in the field (History)
- Optimizing for LiteBIRD
- Designs for optimization
- Conclusions

# LiteBIRD block diagram ver.3 (in TES option)

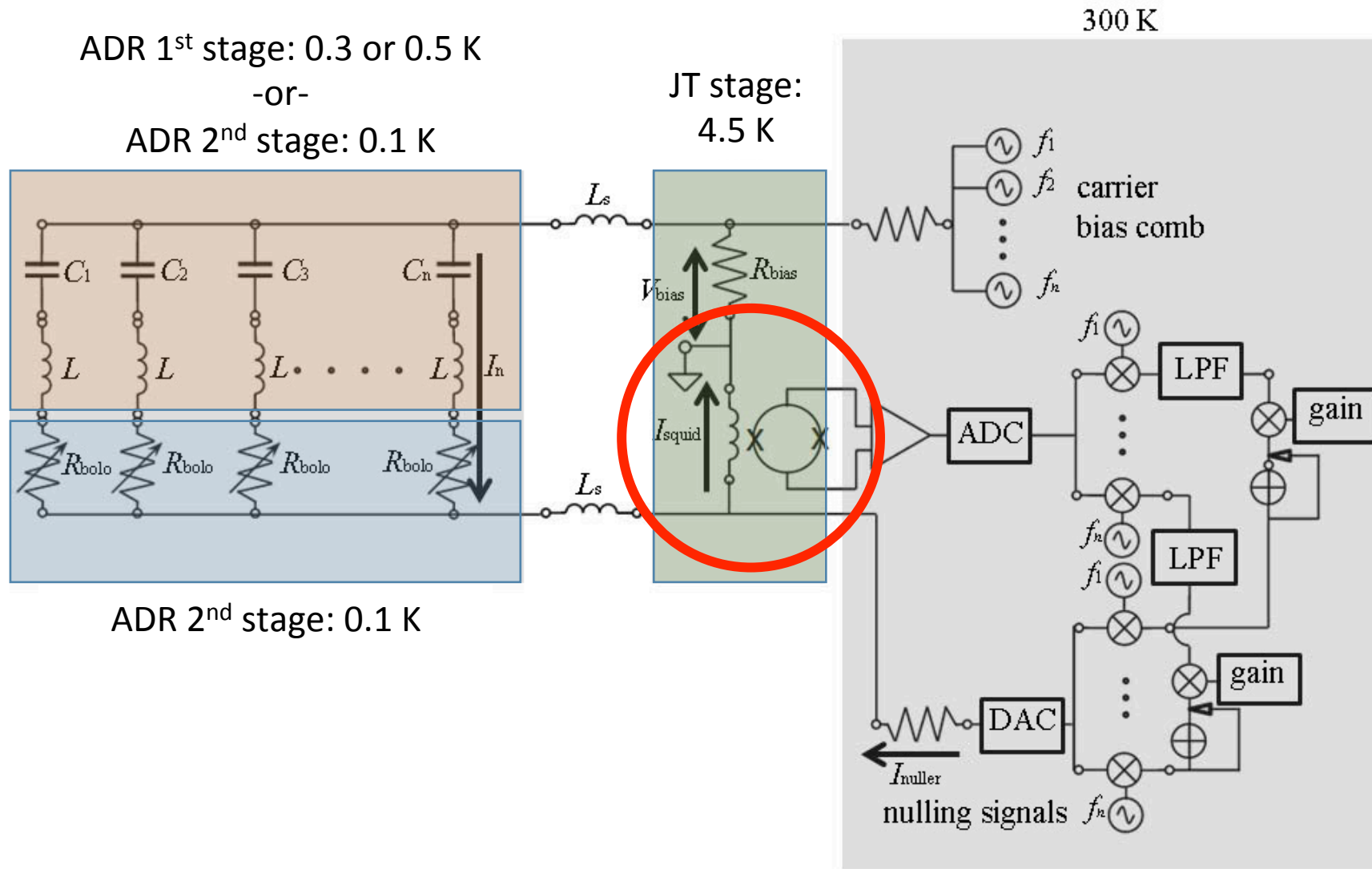
2015-12-1 v1.1e



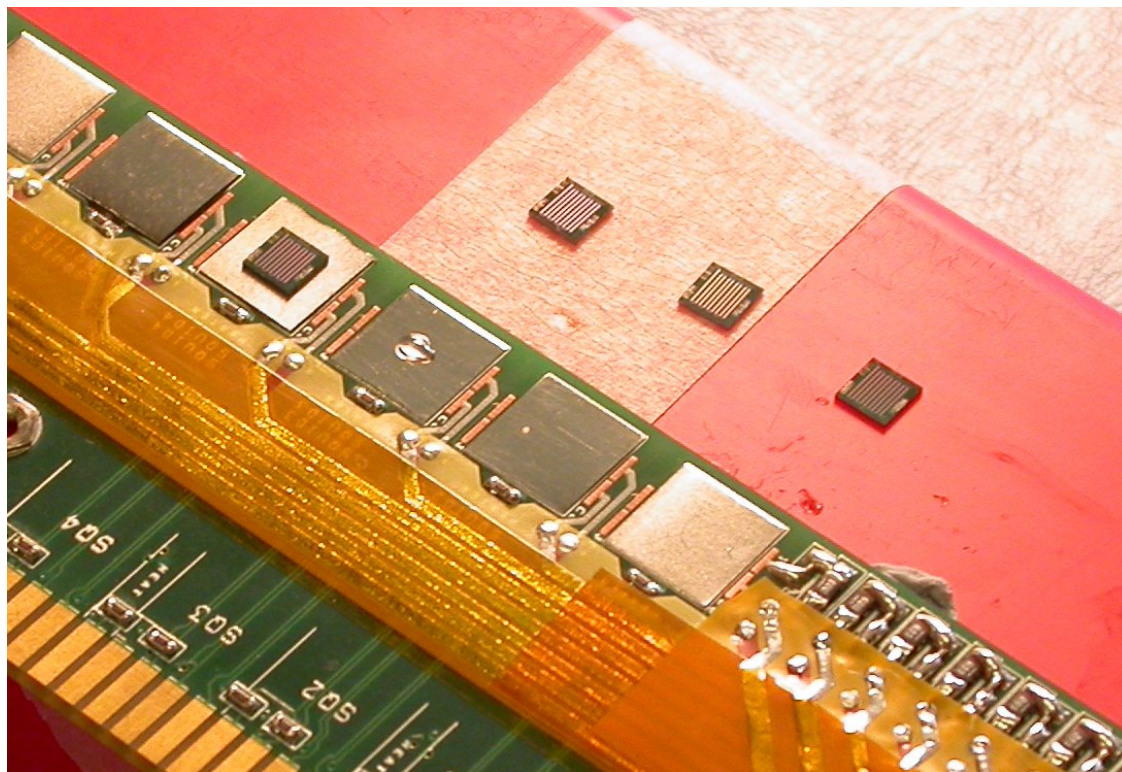
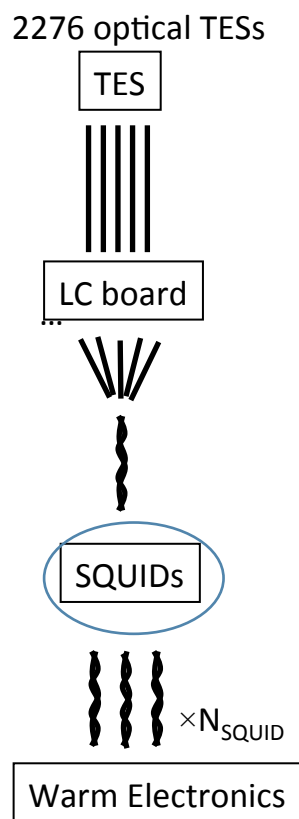
This talk is about optimizing this bit:

The cold SQUIDs and their interaction with wiring

# Readout circuit



# SQUIDs



# SQUIDs for FDM in Satellite CMB Experiments

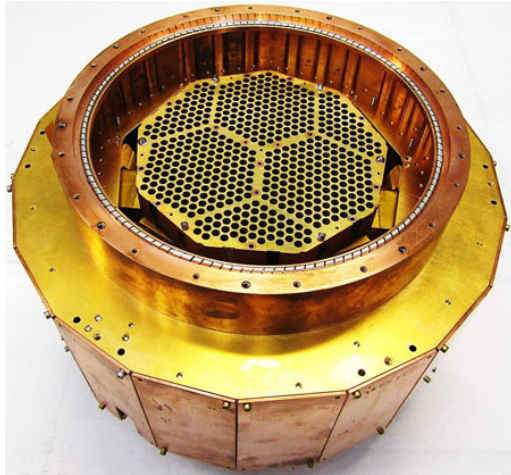
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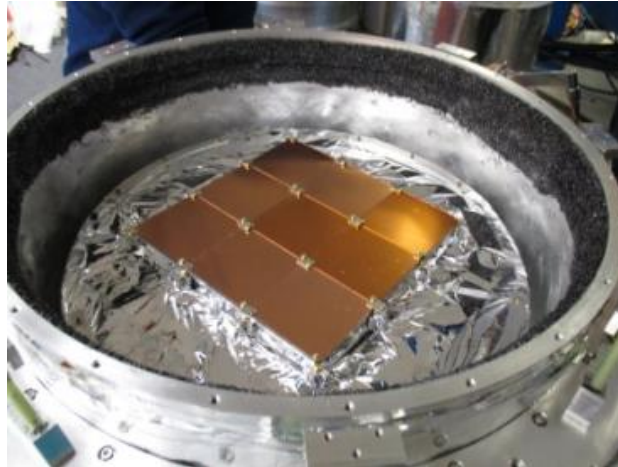


## Some SQUIDs used in CMB polarimeters in the field

ACTpol



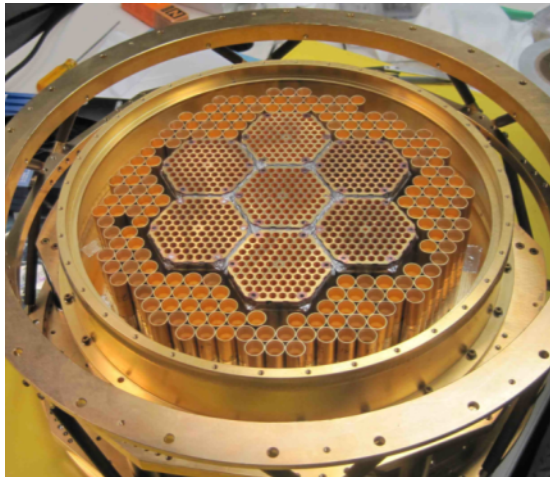
BICEP-3, SPIDER



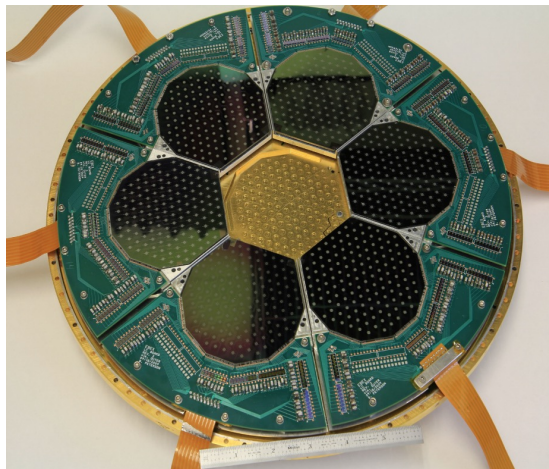
Keck Array



SPTpol



EBEX



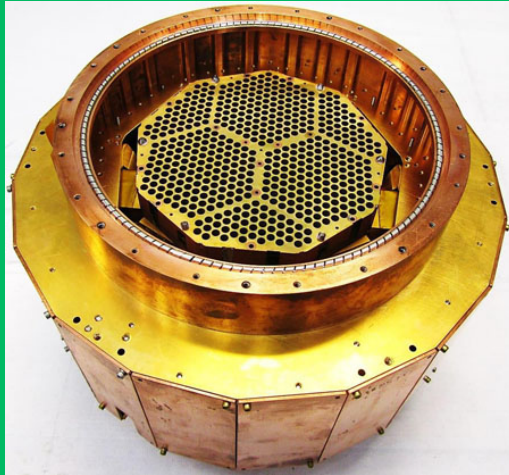
POLARBEAR, Simons



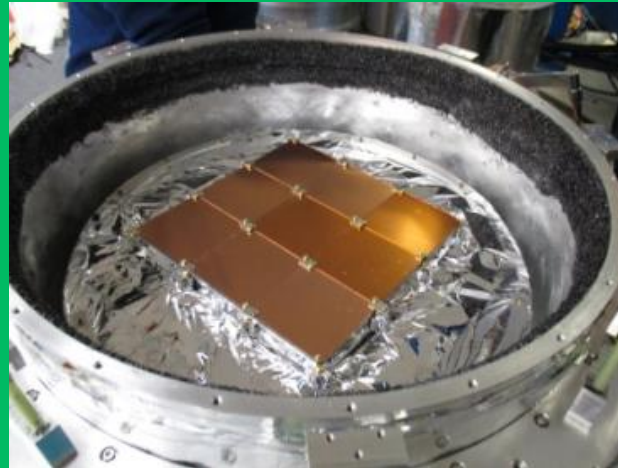


# Some SQUIDs used in CMB polarimeters in the field

ACTpol



BICEP-3, SPIDER

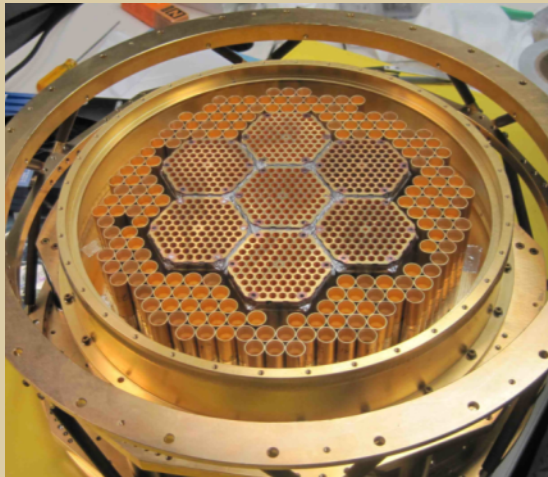


**TDM**

Keck Array

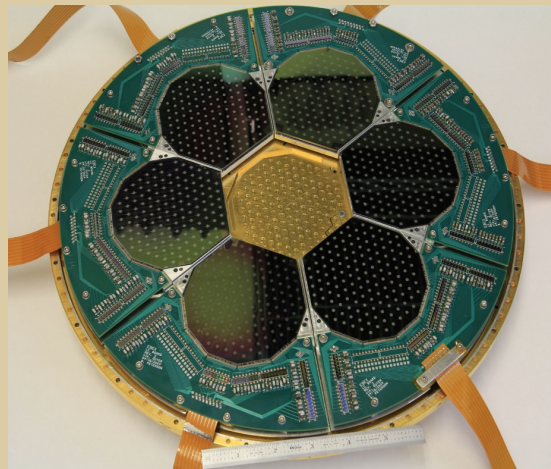


SPTpol



EBEX

**FDM**



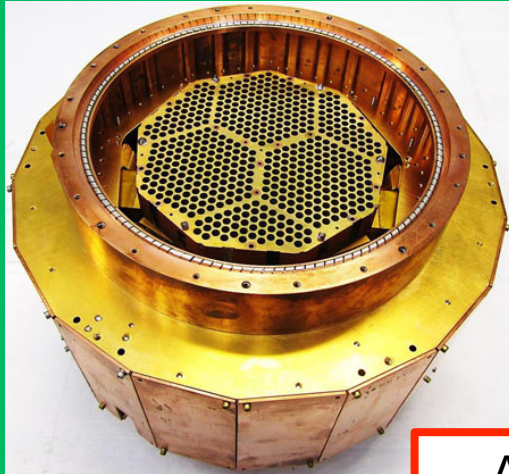
POLARBEAR, Simons



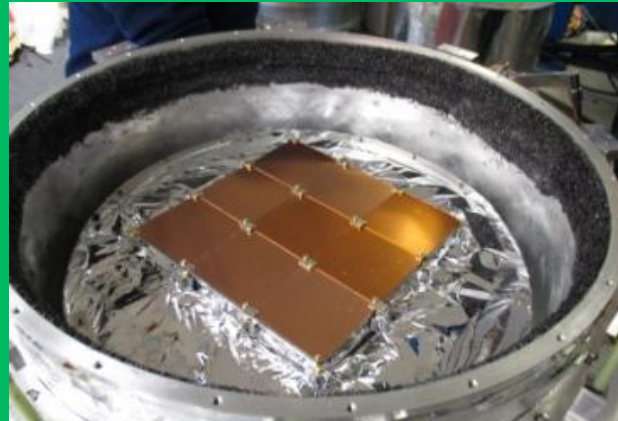


# Some SQUIDs used in CMB polarimeters in the field

ACTpol



BICEP-3, SPIDER



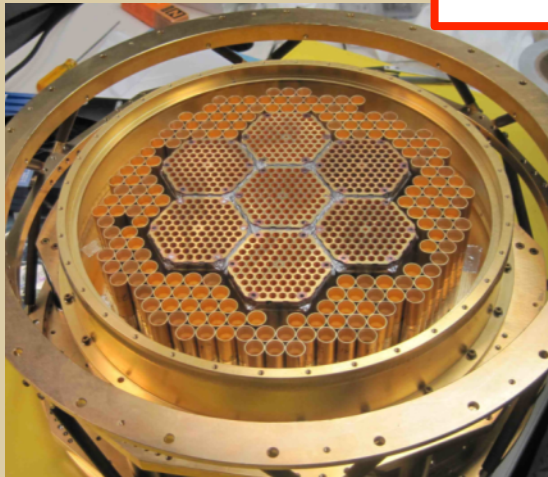
**TDM**

Keck Array

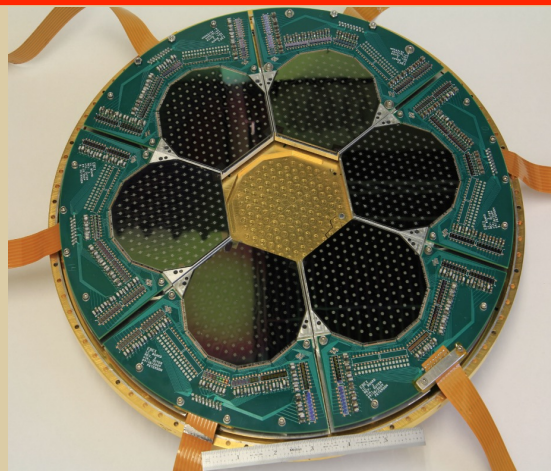


All the SQUIDs used in these experiments were designed and fabricated by members of the LiteBIRD team

SPTpol



EAR, Simons



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# SQUID optimization for LiteBIRD

Design SQUIDs to use the resources available in the satellite platform, with realistic wiring harnesses in the EMI and radiation exposure from the spacecraft and L2 environment

- Power dissipation at each temperature stage
- Dynamic range / noise
- Electromagnetic interference (EMI) sensitivity
- Magnetic field sensitivity
  - a) AC magnetic field pickup in operation
  - b) Flux-trapping sensitivity in initial cooldown (magnet off)
  - c) Flux-trapping sensitivity in mag cycle (magnet on)
  - d) Requirements for flux-expulsion through heating?
- Output impedance / dynamic resistance matched to wiring
  - Determined by wiring harness length, characteristic impedance, normal resistance, and characteristics of room-temperature preamplifier
- Operational temperature of SQUID amplifiers
  - a) 4K
  - b) Intermediate temperature
  - c) Base temperature
  - d) Two-stage

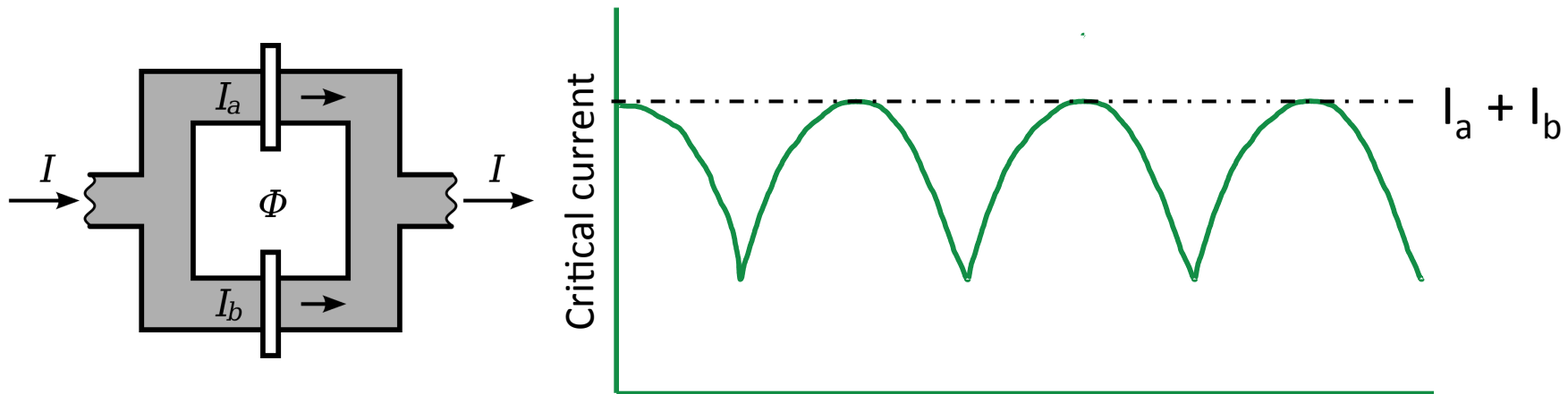
# Tools for SQUID optimization

- Single SQUID design optimization
- Asymmetric SQUIDs (internal self-feedback)
- Gradiometric SQUIDs (series and / or parallel)
- Series-array SQUIDs (for large output voltage)
- Series / Parallel SQUIDs
- Two-stage SQUIDs (one cold single SQUID followed by a series / parallel SQUID at higher temperature)
- SQUIDs with differential output for rejection of common-mode pickup in wiring harness

# dc SQUIDS



- Superconducting Quantum Interference Device (SQUID)
- Invented by Arnold Silver, Ford
- Quantum interference pattern analogous to a two-slit interferometer

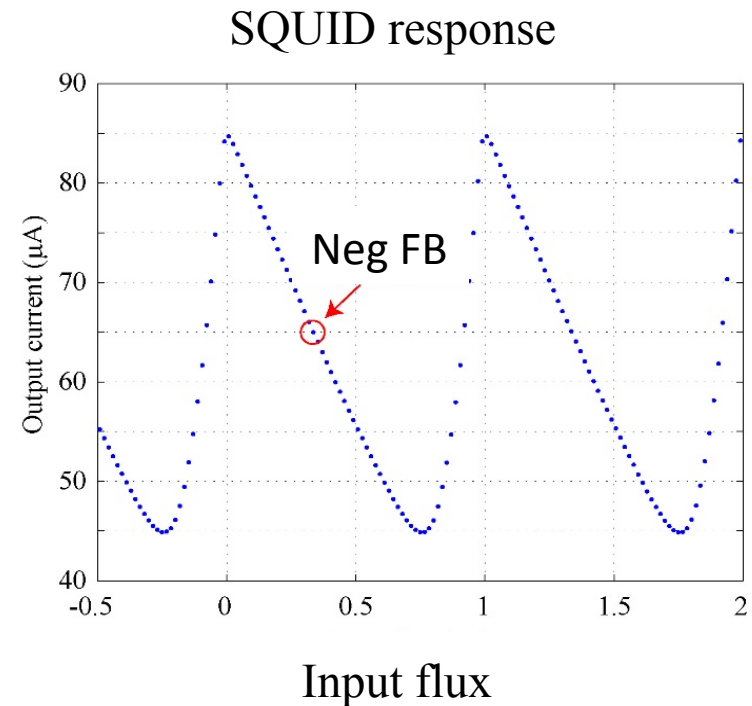
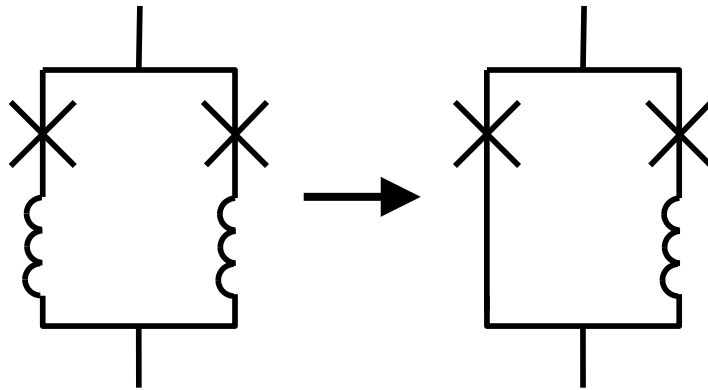


Magnetic flux coupled to SQUID loop

Kent Irwin, Stanford



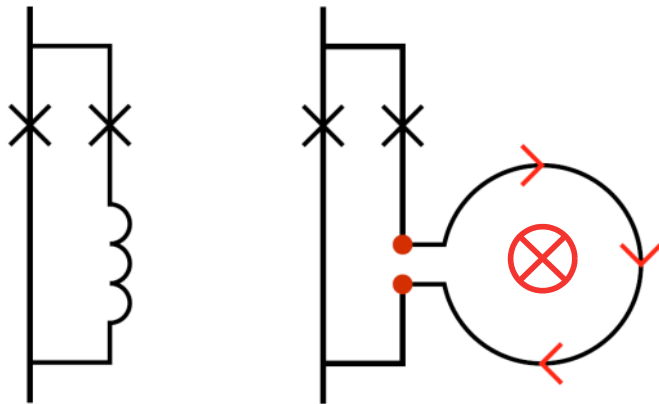
# Asymmetric SQUIDs (Self-feedback)



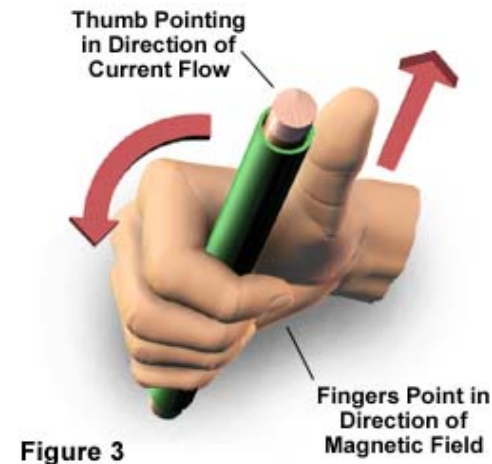
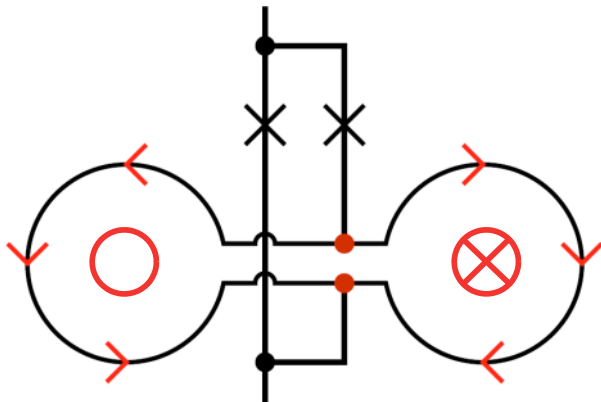
- Put most of the inductance on one side of SQUID loop
- Circulating current in SQUID either enhances (positive feedback) or reduces (negative feedback) the coupled flux.
- Positive feedback: increases output voltage, reduces dynamic range
- Negative feedback: reduced output voltage, increased dynamic range, improved linearity

# Gradiometer SQUIDs for B field insensitivity

Non-gradiometric SQUID



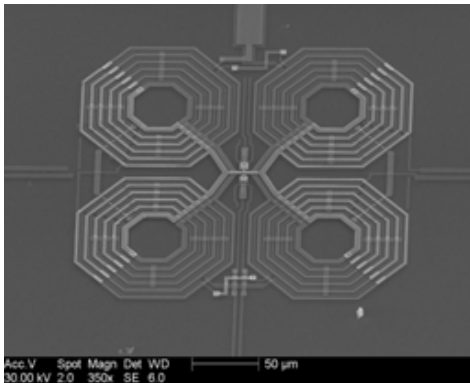
First-order parallel gradiometer



- **Insensitive to uniform B fields**
- Sensitive to first-order B gradients
- **Allows efficient input coils**
- Trapping flux-quantum in coil leads to 180 degree dephasing: only for single SQUIDs

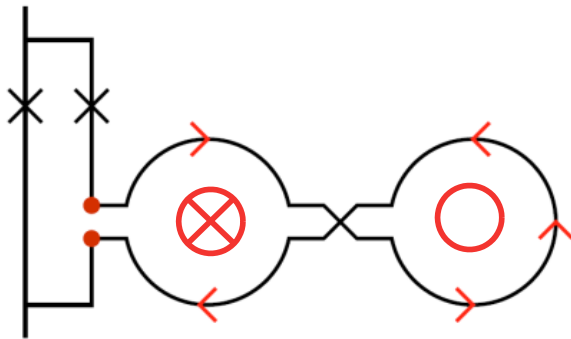
# Gradiometer SQUIDs for B field insensitivity

Second-order parallel gradiometer



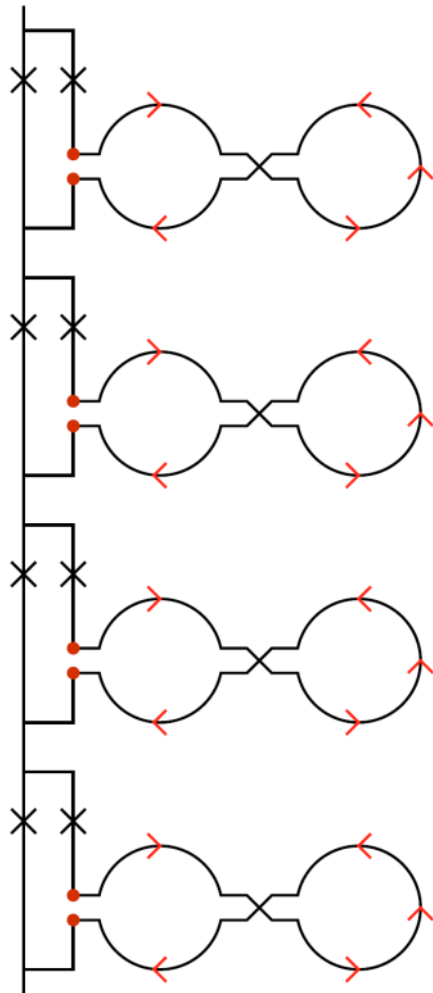
- **Insensitive to uniform B fields**
- **Insensitive to first-order B gradients !!!**
- **Allows efficient input coils**
- Trapping flux-quantum in coil leads to 180 degree dephasing: only for single SQUIDs

First-order serial gradiometer



- **Insensitive to uniform B fields**
- Sensitive to first-order B gradients
- Limited input coil efficiency
- **Doesn't dephase: great for series-array SQUIDs (next)**

# Series-array SQUIDs



With proper engineering, response curve looks like that of a single SQUID

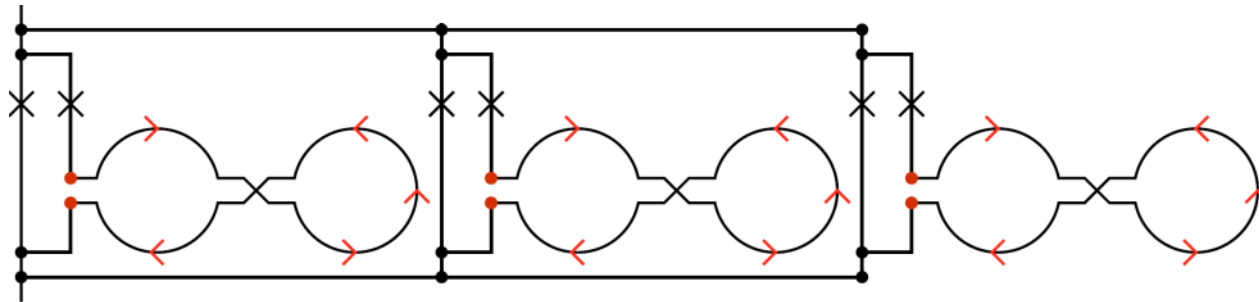
N SQUIDs in series

- **N times higher output voltage**
- **$\sqrt{N}$  times higher signal-to-noise ratio**
- N times higher dynamic resistance
- N times higher power dissipation

Must use serial gradiometer to prevent dephasing

*Increases output voltage swing*

# Parallel-array SQUIDs



With proper engineering, response curve looks like that of a single SQUID

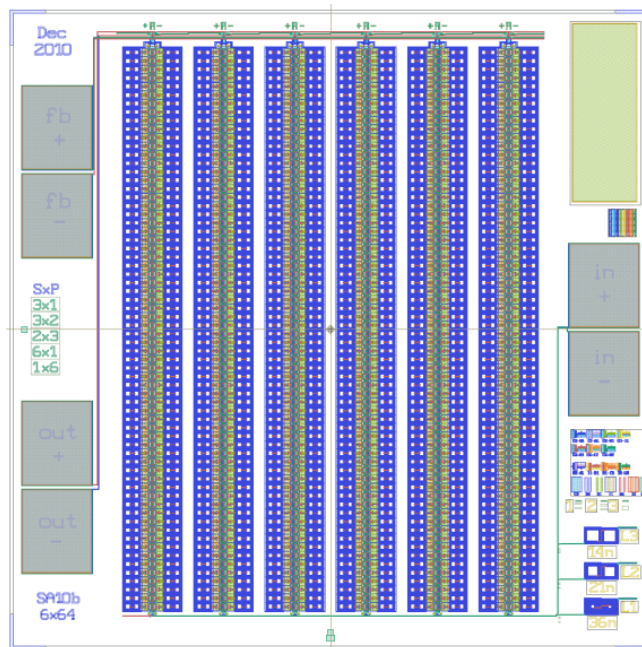
M SQUIDs in parallel

- **$\sqrt{M}$  times higher signal-to-noise ratio**
- **M times lower dynamic resistance**
- M times higher power dissipation

Must use serial gradiometer to prevent dephasing

*Reduces output dynamic resistance*

# Parallel / Series array SQUIDs



2 x 192 (parallel x series) SQUID  
array design deployed on BICEP-3

*Increases output voltage and reduces output dynamic resistance*



# Conclusion

- Further optimization possible:
  1. Two-stage SQUID (first stage at base temperature, SA SQUID at 4K)
  2. Differential output from SA and differential preamp: insensitive to common-mode pickup in wiring harness
- Requirements for SQUIDs are being established
- SQUID specifications can be optimized for LiteBIRD requirements and resources