

T. Matsumura (ISAS/JAXA)

# **CMB telescope and the design consideration toward a next generation satellite mission**

# Introduction

- Design of the optical system
- Heritage of the past CMB telescopes
- Design consideration toward the next space mission

# Design of the optical system

The list of the requirements and constraints to design the optical system to the next generation CMB telescope.

## Requirements from science

- Beam size
- Field-of-view
- Observing band
- Beam qualities
  - Main lobe
  - Near-sidelobe
  - Far-sidelobe
- Beam calibration capability
- Temperature

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## Potential constraints

- Size (mirror/lens/filters/HWP...)
- Telecentric focal plane
- Available mount
- Cooling capability
- Where to define the aperture
- Mass
- Power
- Budget

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## Design parameters

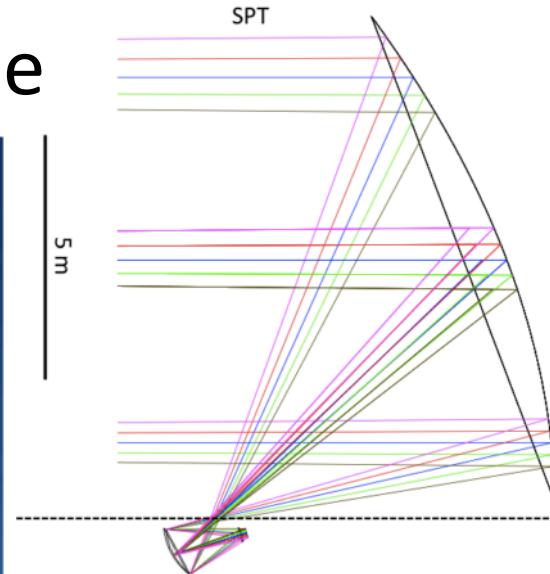
- Aperture size
- F/#
- The # of optical elements and its shapes
- Feed
- ...

B-mode from space

# Examples of the optical system

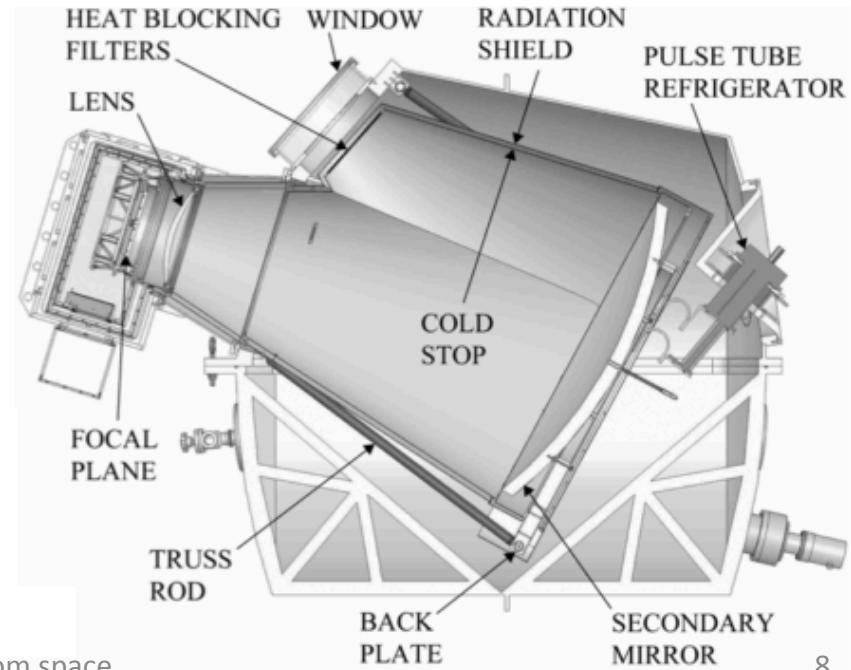


# South Pole Telescope



|   | ACT  | SPT  |
|---|------|------|
| $D_p$ (m)                                 | 6    | 10   |
| $D_i$ (m)                                 | 5.6  | 7.5  |
| $D_s$ (m)                                 | 2    | 1    |
| $F_G$                                     | 2.5  | 1.3  |
| Temperature Receivers                     |      |      |
| $F_{temp}$                                | 0.9  | 1.3  |
| $F_{\lambda_{150}}$                       | 0.5  | 1.7  |
| $A\Omega_{R_{temp}}$ (cm <sup>2</sup> sr) | 40   | 105  |
| $A\Omega_{D_{eff}}$ (relative)            | ~2.5 | 1    |
| Min. Strehl <sub>150</sub>                | 0.97 | 0.89 |
| FWHM <sub>150</sub> (arcmin)              | 1.37 | 1.15 |
| Polarization Receivers                    |      |      |
| $F_{pol}$                                 | 1.4  | 1.3  |
| $F_{\lambda_{150}}$                       | 1.4  | 1.6  |
| $A\Omega_{R_{pol}}$ (cm <sup>2</sup> sr)  | 180  | 140  |

## SPT Receiver Overview

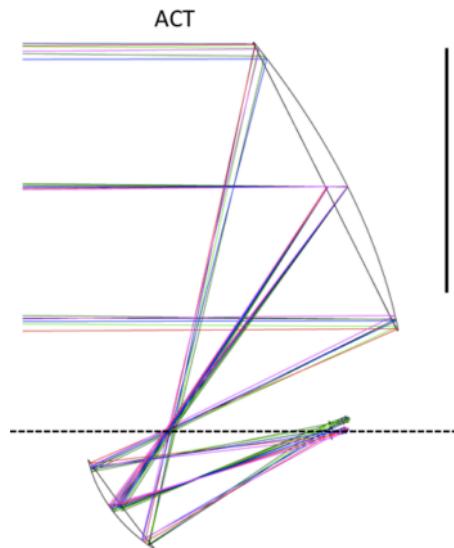


|                       | ACT                  | SPT                             |
|-----------------------|----------------------|---------------------------------|
| Primary shape         | Ellipsoid            | Paraboloid                      |
| Easily reconfigurable | No                   | Yes                             |
| Stop type             | Primary image        | Secondary reflector             |
| Cold stop Temperature | 1 Kelvin             | 10 Kelvin                       |
| Refractive optics     | HDPE lens            | Conical feedhorns               |
| Temp. array coupling  | Filled focal plane   | Corrugated & profiled feedhorns |
| Pol. array coupling   | Corrugated feedhorns |                                 |

December 15, 2015

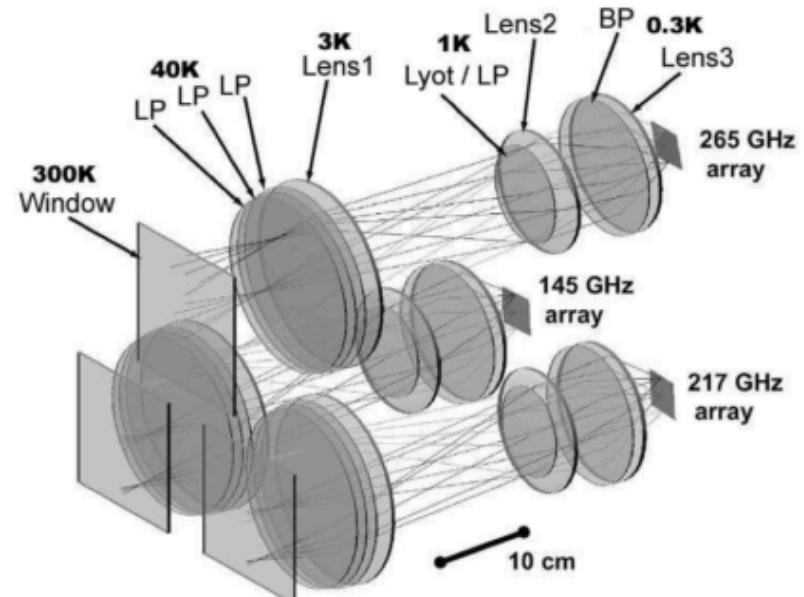
B-mode from space

# Atacama Cosmology Telescope (ACT)



|   | ACT  | SPT  |
|---|------|------|
| $D_p$ (m)                                 | 6    | 10   |
| $D_i$ (m)                                 | 5.6  | 7.5  |
| $D_s$ (m)                                 | 2    | 1    |
| $F_G$                                     | 2.5  | 1.3  |
| Temperature Receivers                     |      |      |
| $F_{temp}$                                | 0.9  | 1.3  |
| $F\lambda_{150}$                          | 0.5  | 1.7  |
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| Min. Strehl <sub>150</sub>                | 0.97 | 0.89 |
| FWHM <sub>150</sub> (arcmin)              | 1.37 | 1.15 |
| Polarization Receivers                    |      |      |
| $F_{pol}$                                 | 1.4  | 1.3  |
| $F\lambda_{150}$                          | 1.4  | 1.6  |
| $A\Omega_{R_{pol}}$ (cm <sup>2</sup> sr)  | 180  | 140  |

## ACT Receiver Optics

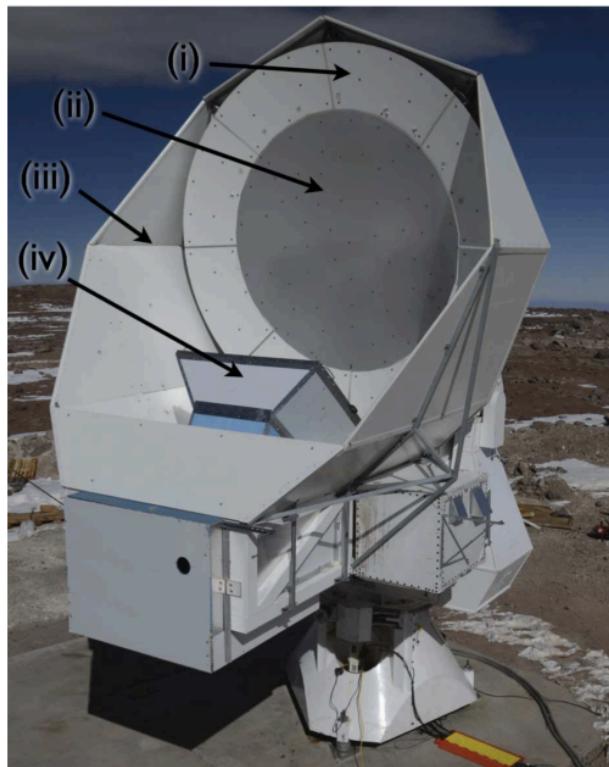


|                       | ACT                        | SPT                             |
|-----------------------|----------------------------|---------------------------------|
| Primary shape         | Ellipsoid                  | Paraboloid                      |
| Easily reconfigurable | No                         | Yes                             |
| Stop type             | Primary image              | Secondary reflector             |
| Cold stop Temperature | 1 Kelvin                   | 10 Kelvin                       |
| Refractive optics     | 3 Silicon lenses per array | HDPE lens                       |
| Temp. array coupling  | Filled focal plane         | Conical feedhorns               |
| Pol. array coupling   | Corrugated feedhorns       | Corrugated & profiled feedhorns |

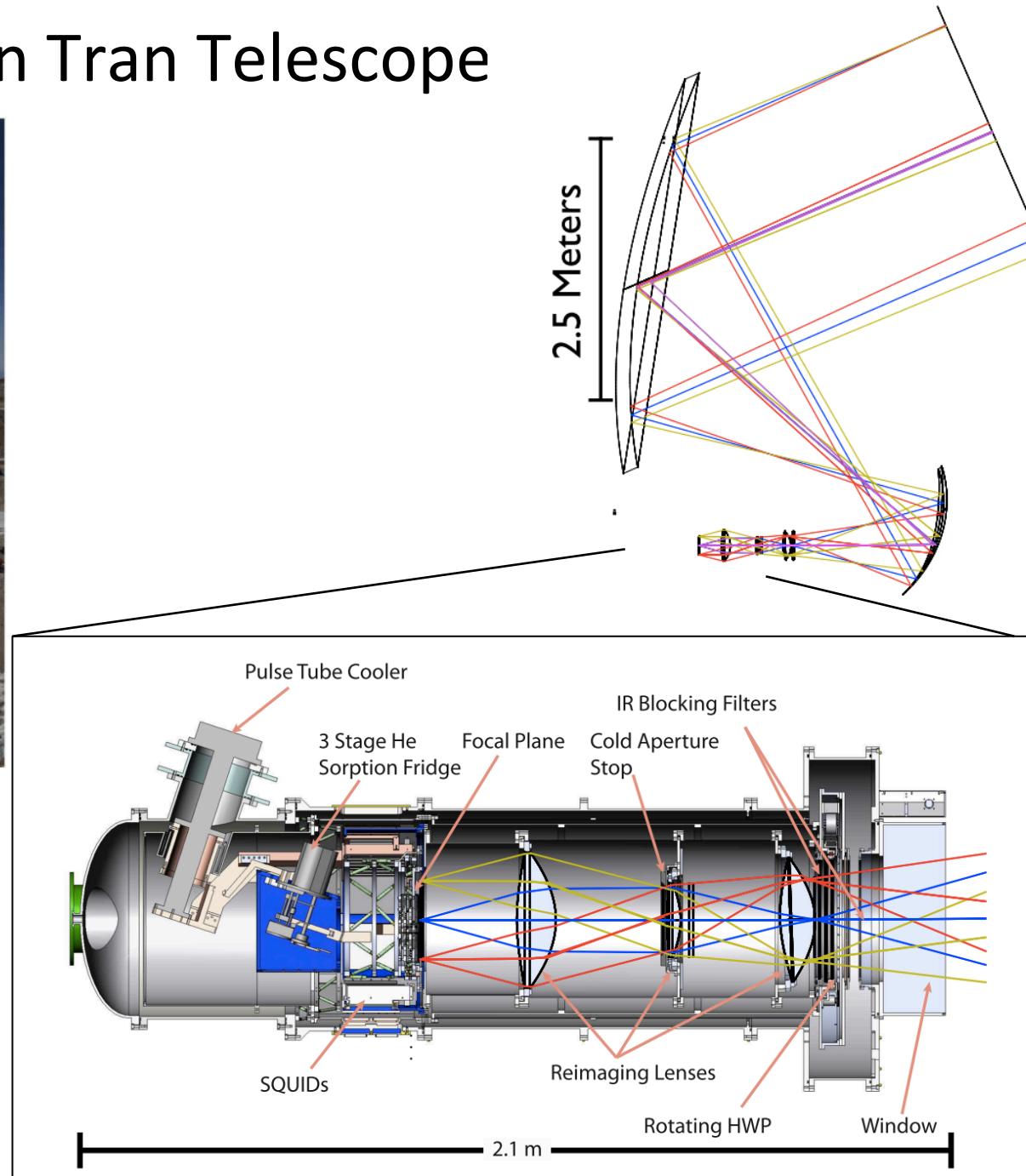
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B-mode from space

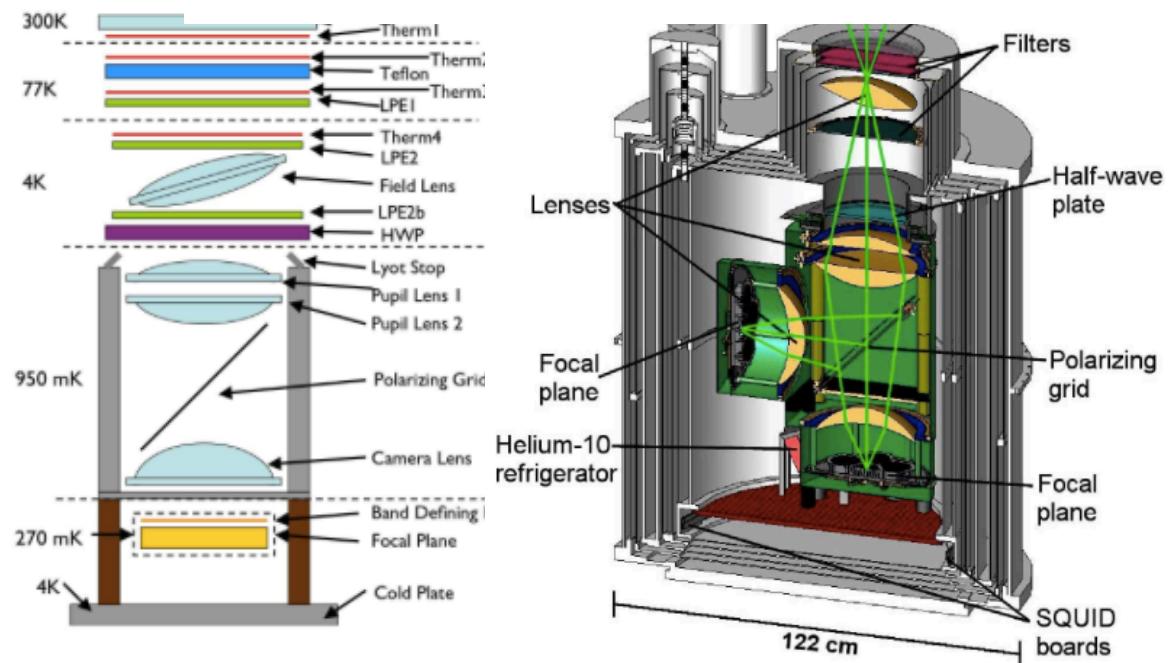
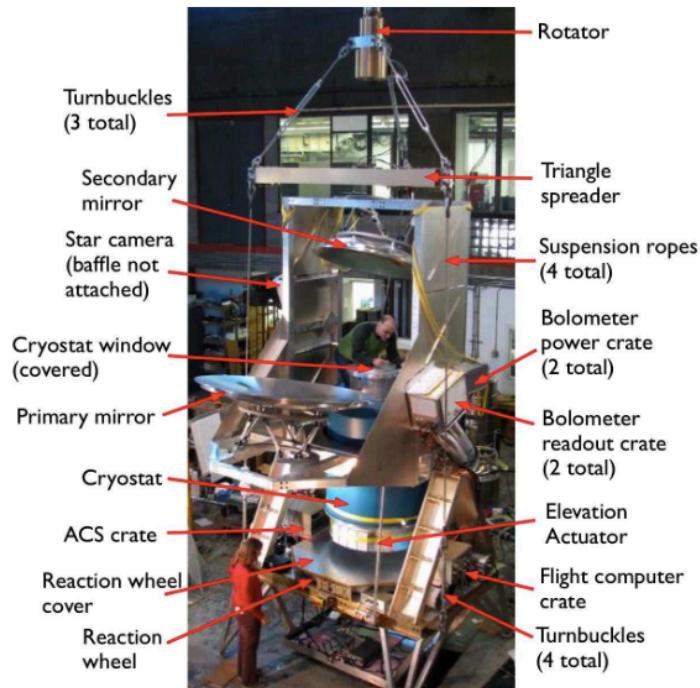
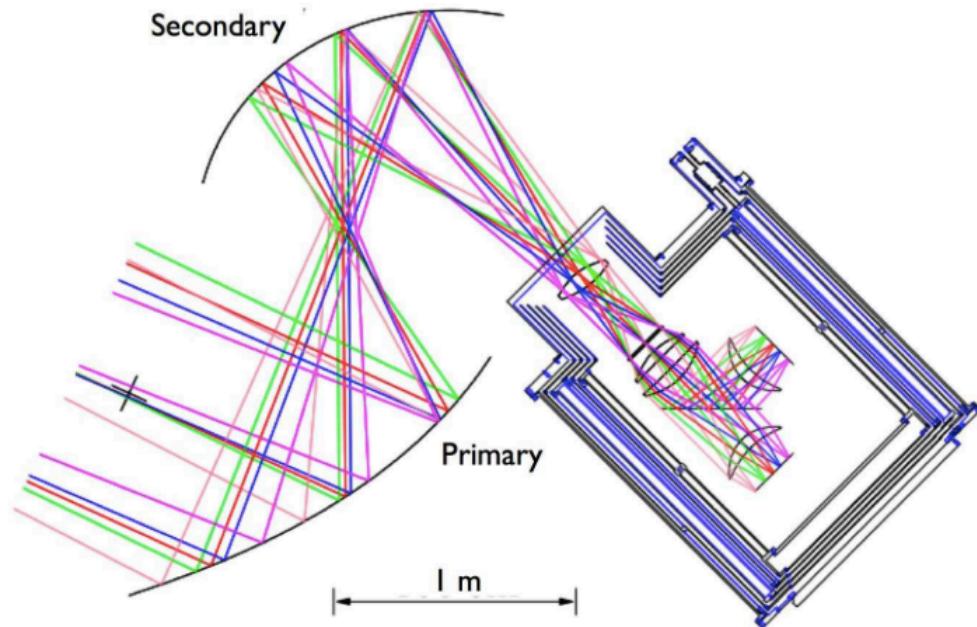
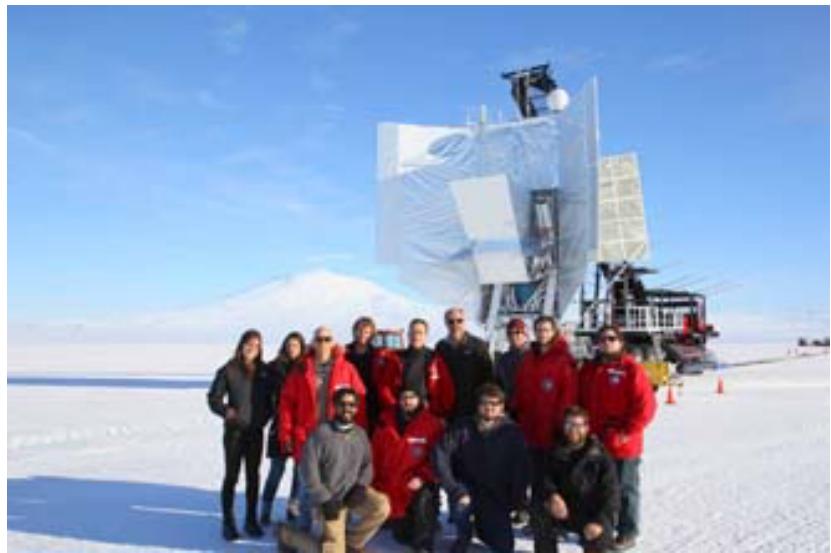
# POLARBEAR Huan Tran Telescope



December 15, 2015

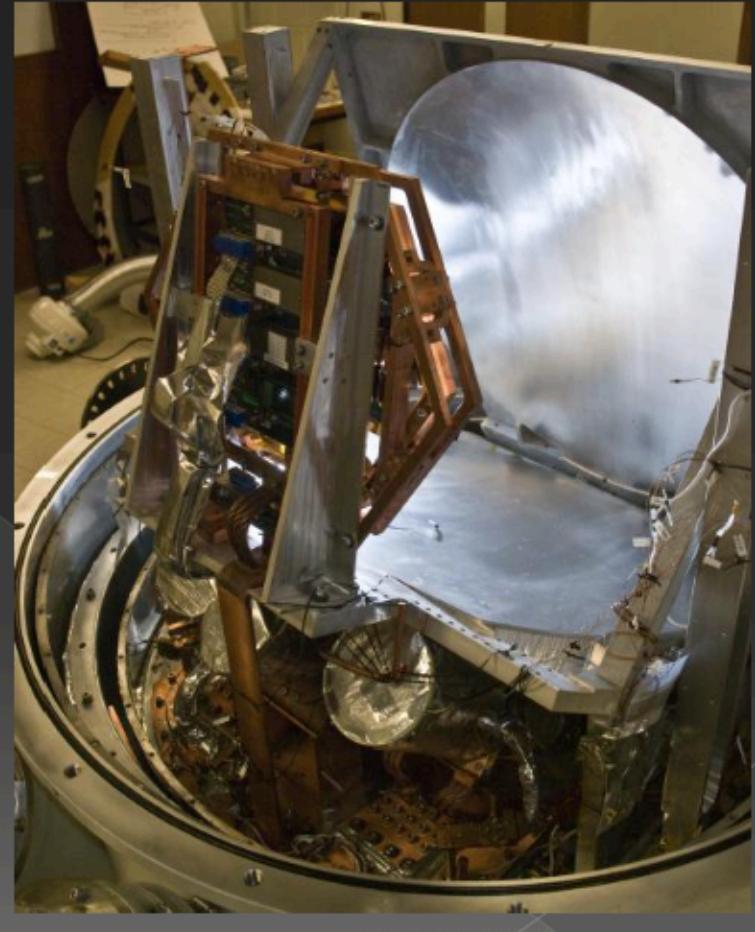
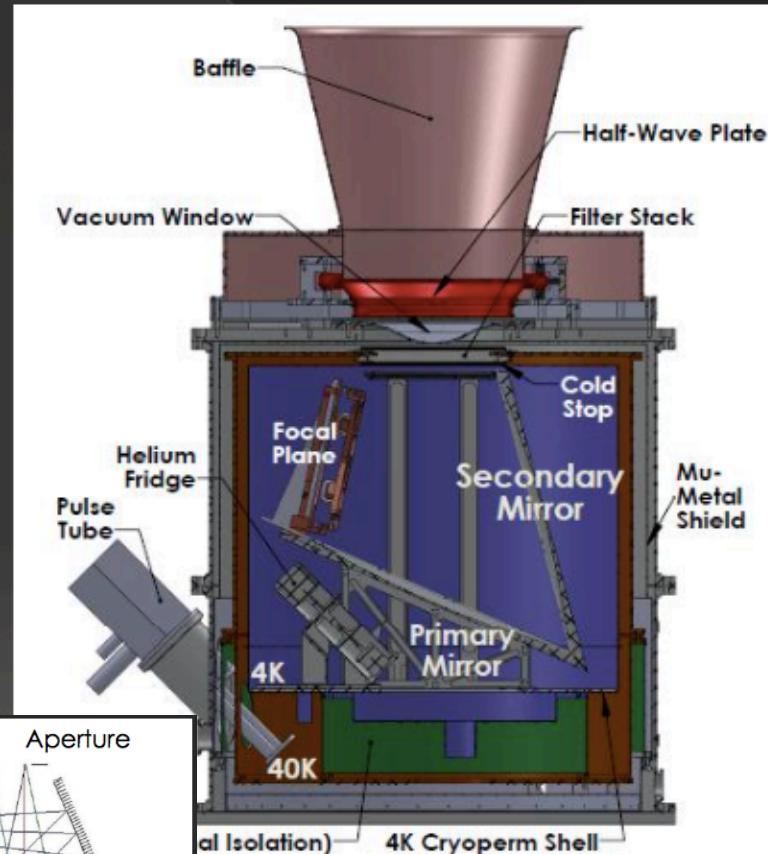
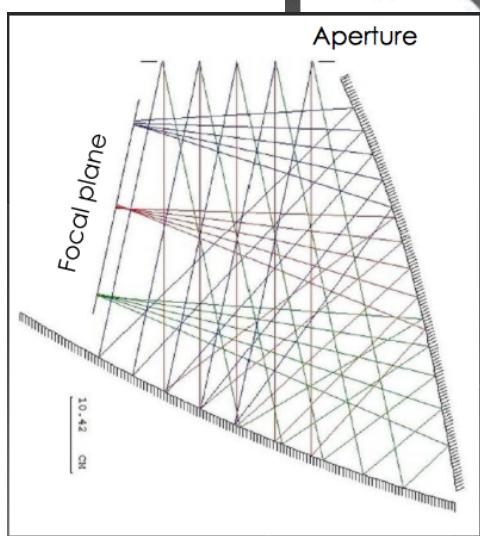


# EBEX



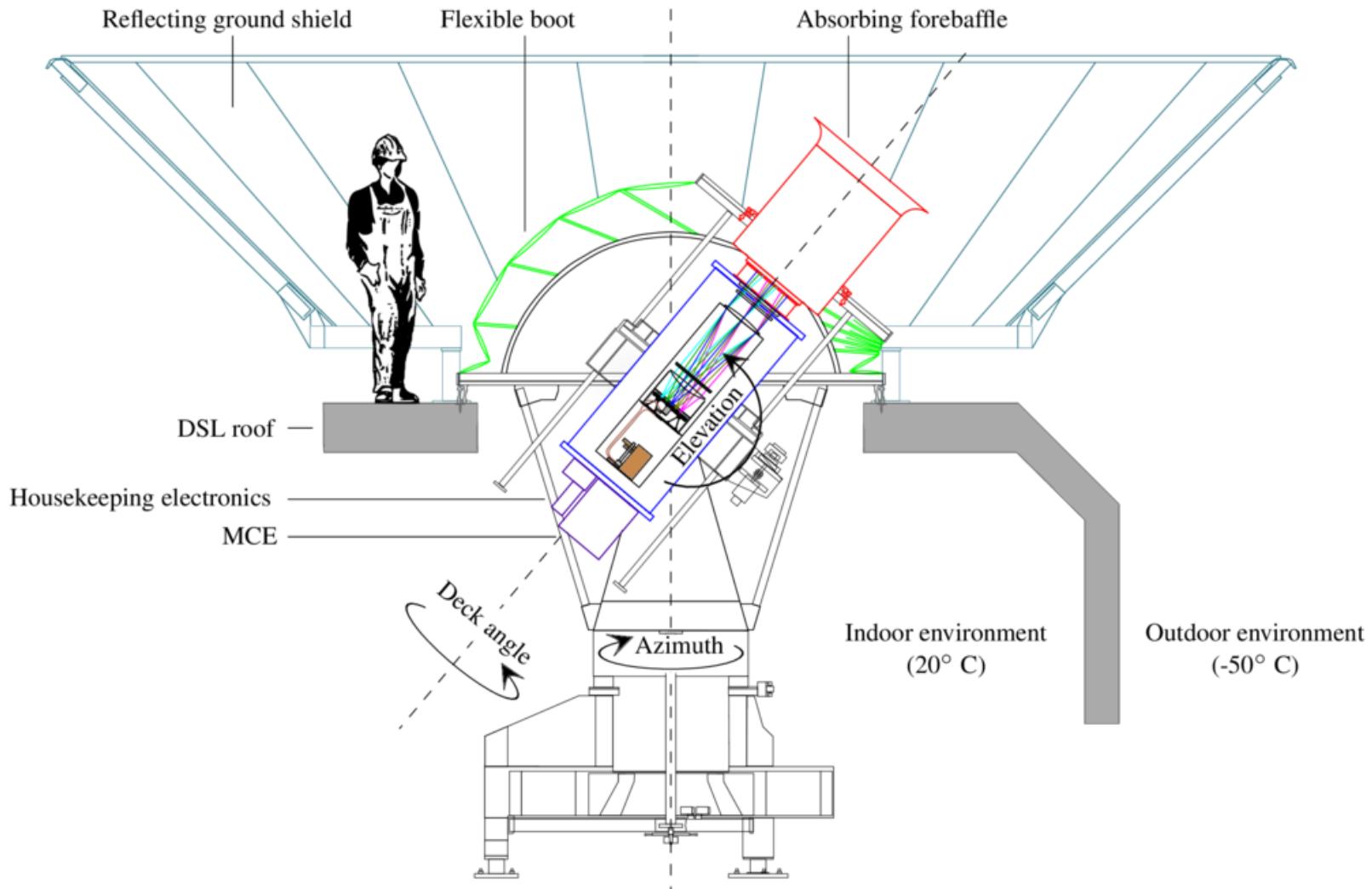
# ABS

## Optics

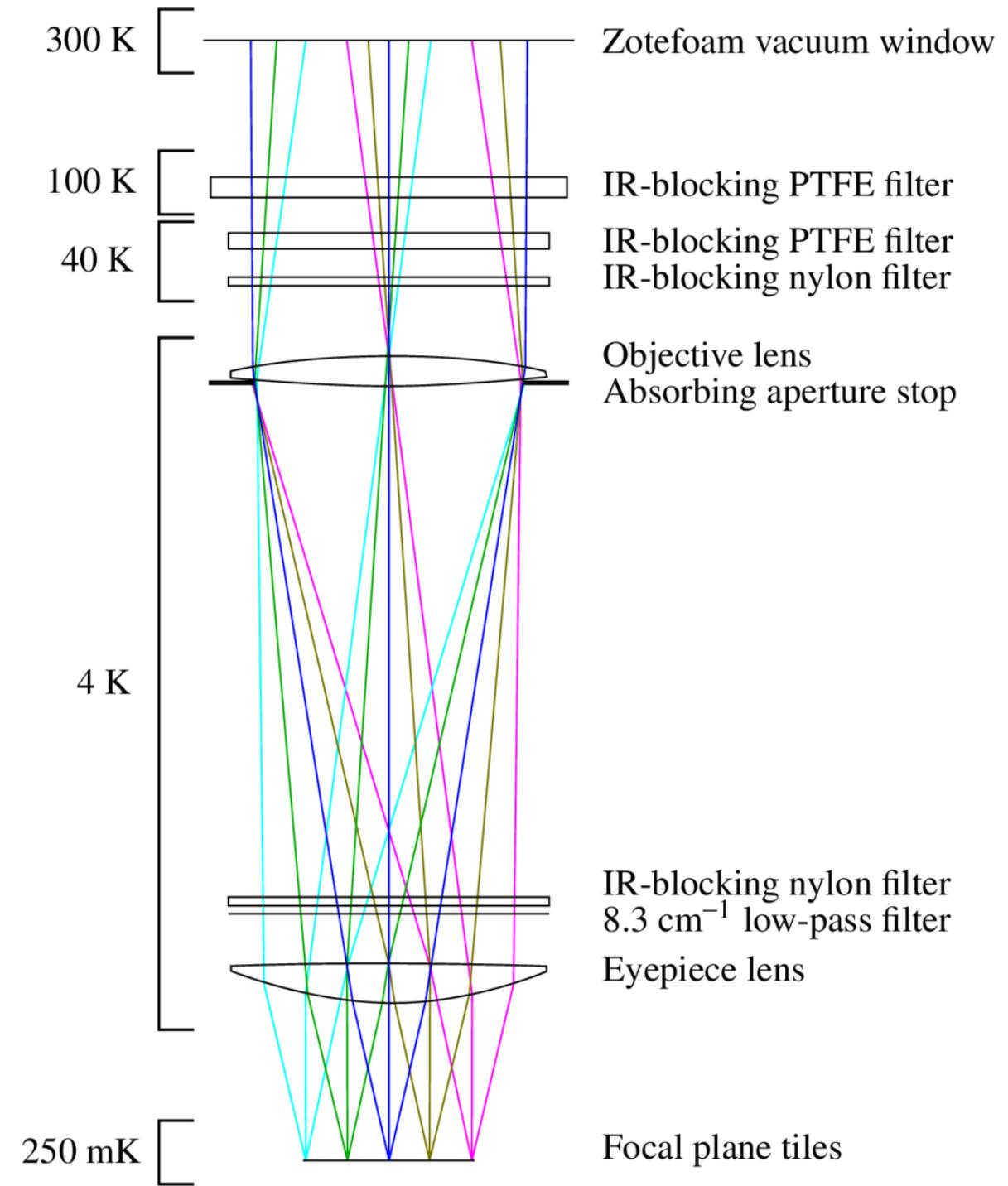


B-mode from space

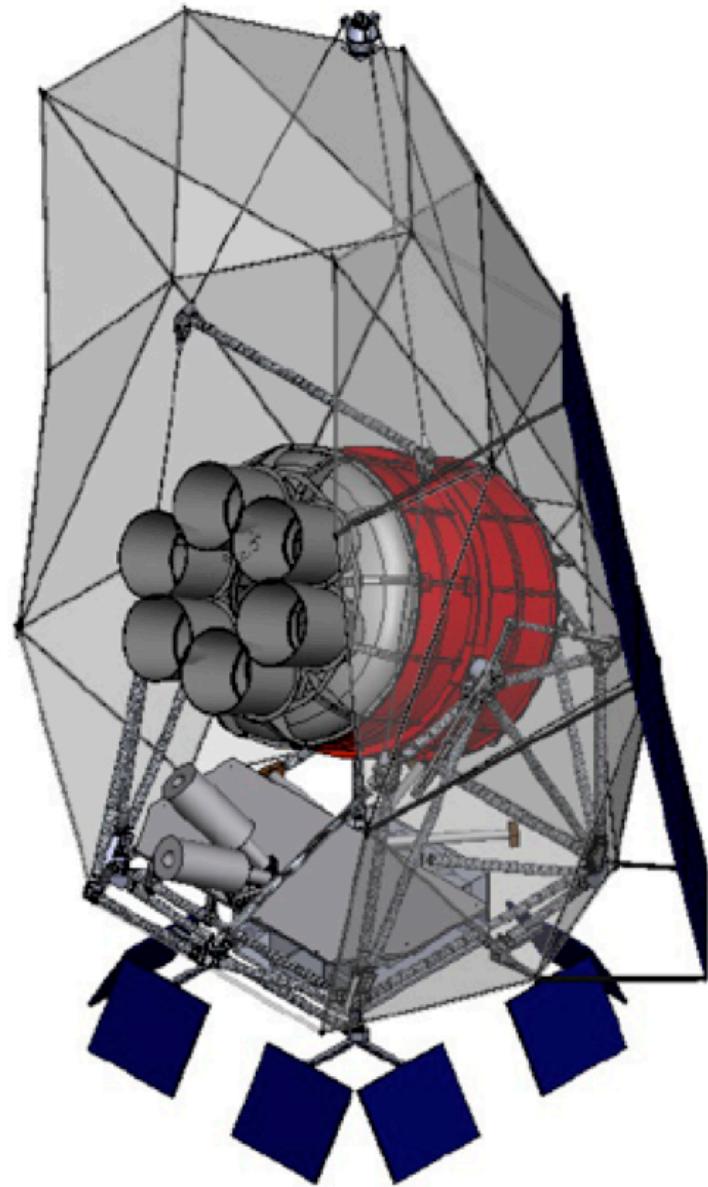
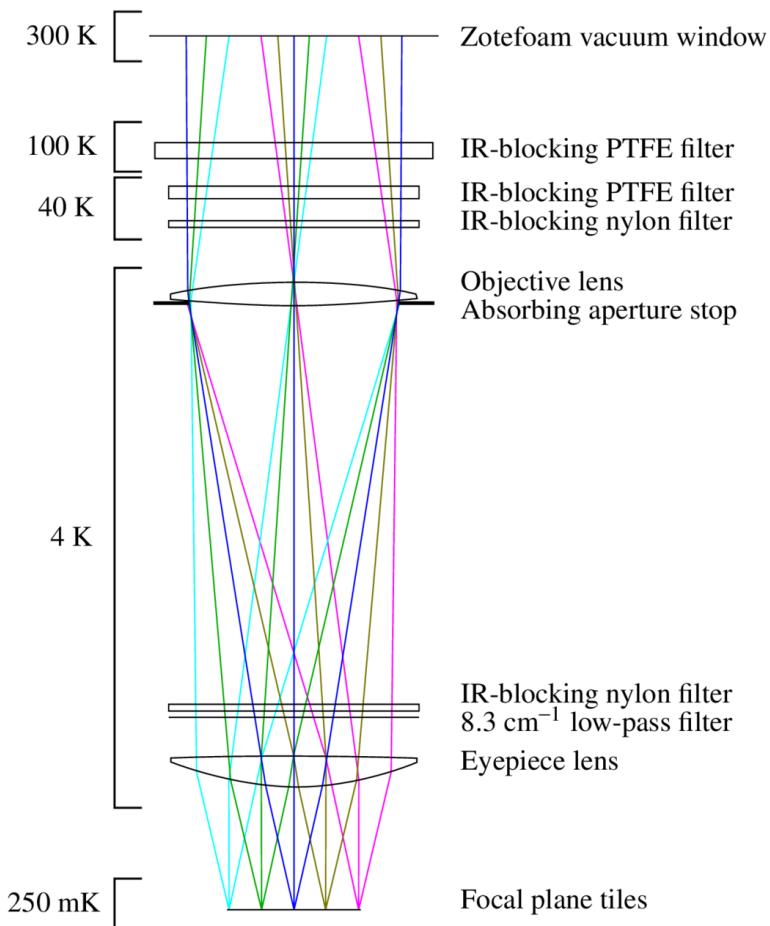
# BICEP



# BICEP/KECK



# SPIDER



# BICEP3

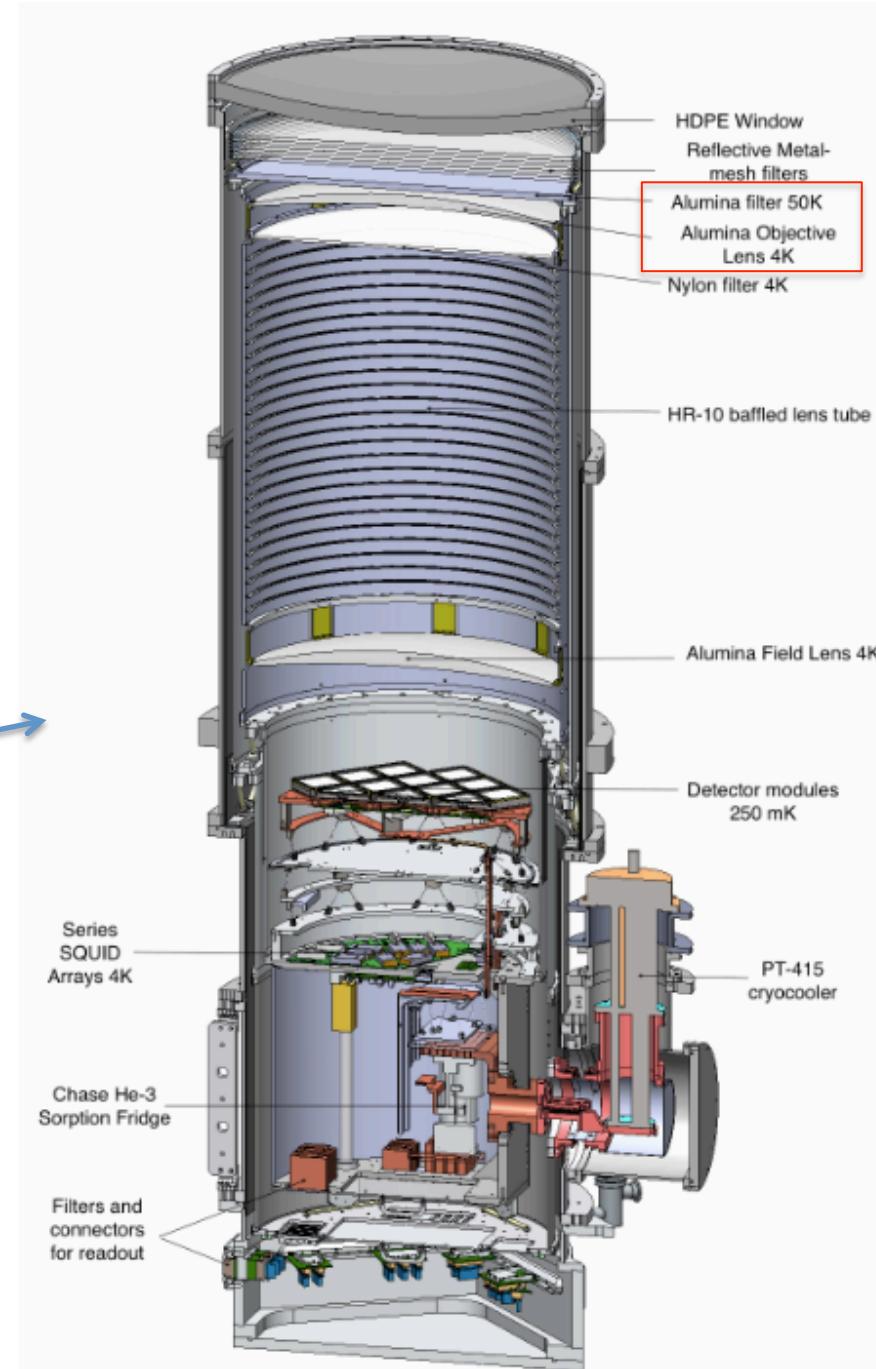
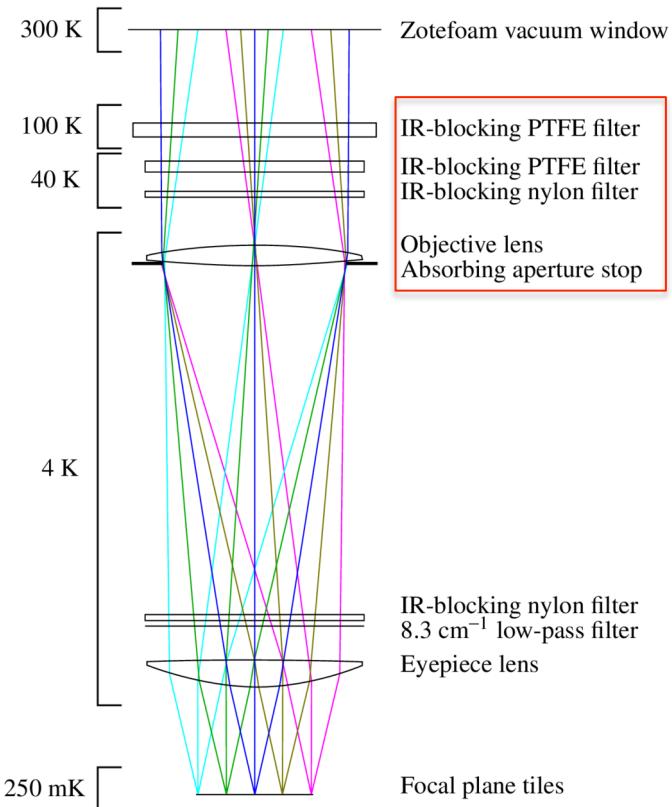
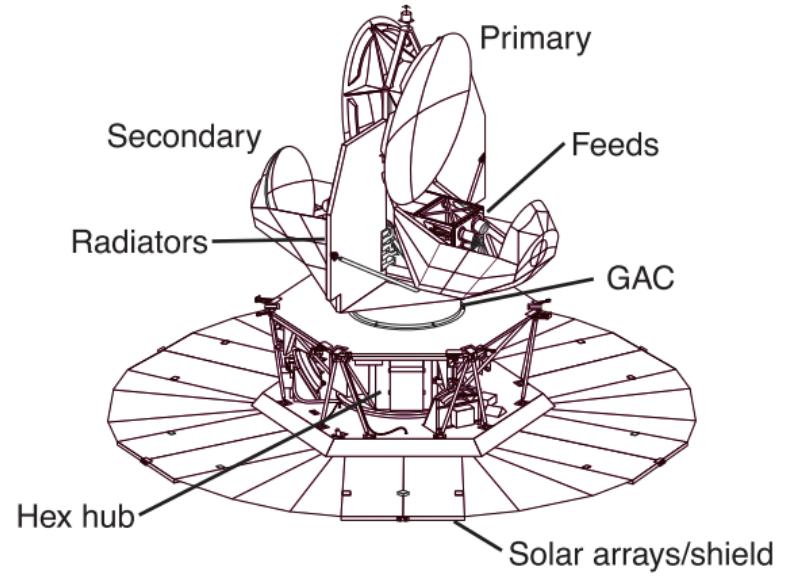
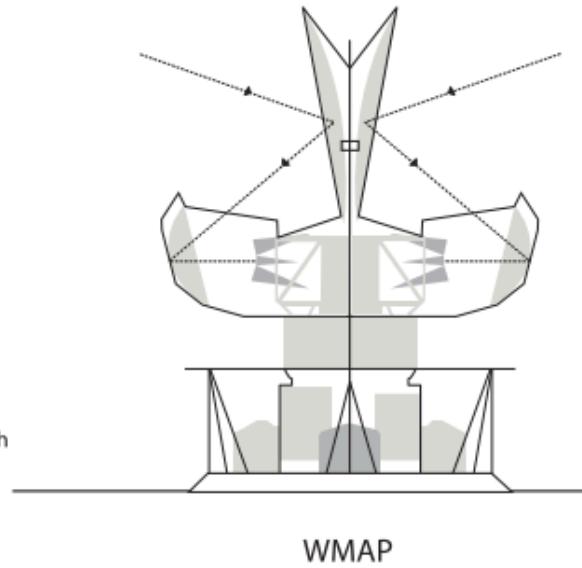
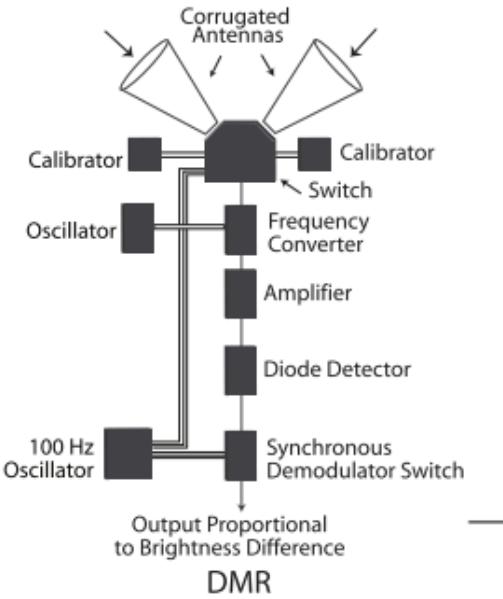
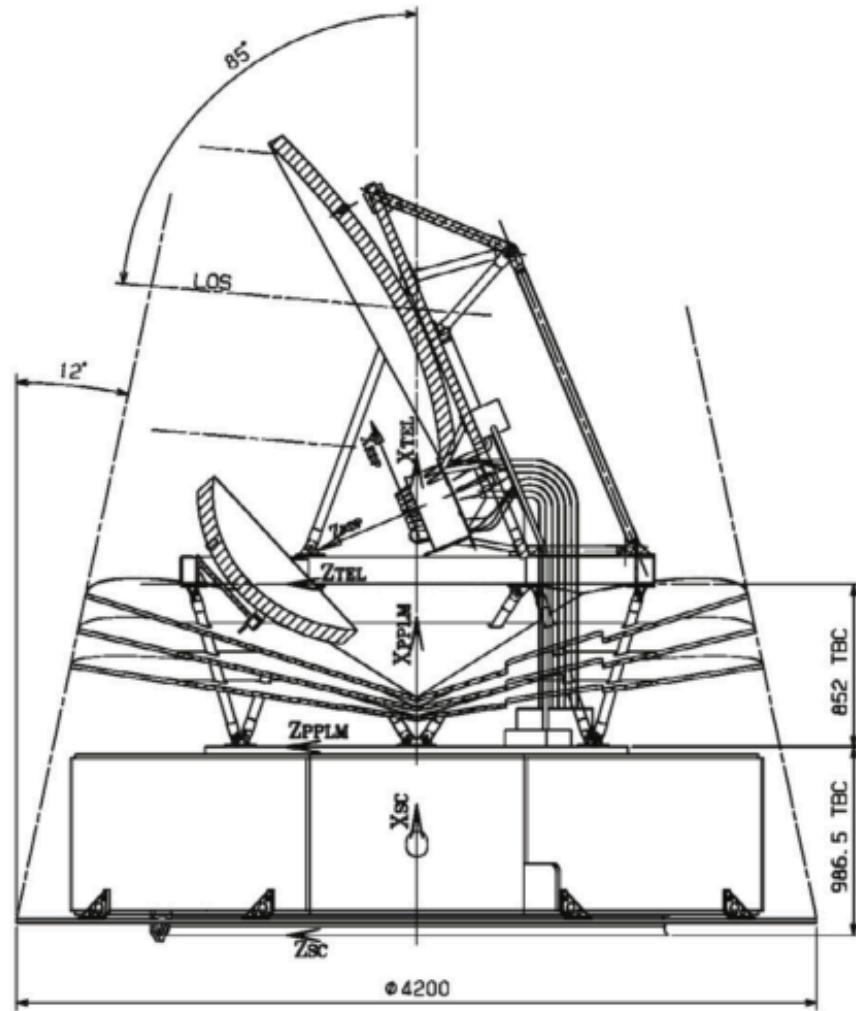


Figure 3. Cross section of BICEP3 receiver showing various components.



|       | Relikt (1983) |   |    |                       | COBE (1989) |   |    |                       | WMAP (2001) |   |      |                       | Planck (2009) |       |        |                       |
|-------|---------------|---|----|-----------------------|-------------|---|----|-----------------------|-------------|---|------|-----------------------|---------------|-------|--------|-----------------------|
|       | Freq<br>GHz   | N | S  | $\theta_{1/2}$<br>deg | Freq<br>GHz | N | S  | $\theta_{1/2}$<br>deg | Freq<br>GHz | N | S    | $\theta_{1/2}$<br>deg | Freq<br>GHz   | N     | S      | $\theta_{1/2}$<br>deg |
| Decem | 37.5          | 1 | 25 | 5.8°                  | 31.5        | 2 | 30 | 7°                    | 22.7        | 2 | 0.49 | 0.82°                 | 28.5          | 4     | 0.15   | 0.54°                 |
|       |               |   |    |                       | 53          | 2 | 11 | 7°                    | 33.0        | 2 | 0.51 | 0.62°                 | 40.7          | 4     | 0.47   | 0.49°                 |
|       |               |   |    |                       | 90          | 2 | 16 | 7°                    | 40.7        | 4 | 0.47 | 0.49°                 | 60.6          | 4     | 0.54   | 0.33°                 |
|       |               |   |    |                       |             |   |    |                       | 60.6        | 4 | 0.54 | 0.33°                 | 44.1          | 6     | 0.16   | 0.47°                 |
|       |               |   |    |                       |             |   |    |                       | 93.4        | 8 | 0.58 | 0.21°                 | 70.3          | 12    | 0.13   | 0.22°                 |
|       |               |   |    |                       |             |   |    |                       |             |   |      |                       | 100           | 8/4P  | 0.0173 | 0.16°                 |
|       |               |   |    |                       |             |   |    |                       |             |   |      |                       | 143           | 12/4P | 0.0084 | 0.12°                 |
|       |               |   |    |                       |             |   |    |                       |             |   |      |                       | 217           | 12/4P | 0.0068 | 0.078°                |
|       |               |   |    |                       |             |   |    |                       |             |   |      |                       | 353           | 12/4P | 0.0055 | 0.074°                |
|       |               |   |    |                       |             |   |    |                       |             |   |      |                       | 545           | 4     | 0.0045 | 0.063°                |
|       |               |   |    |                       |             |   |    |                       |             |   |      |                       | 857           | 4     | 0.0019 | 0.061°                |

# Planck: See the next talk



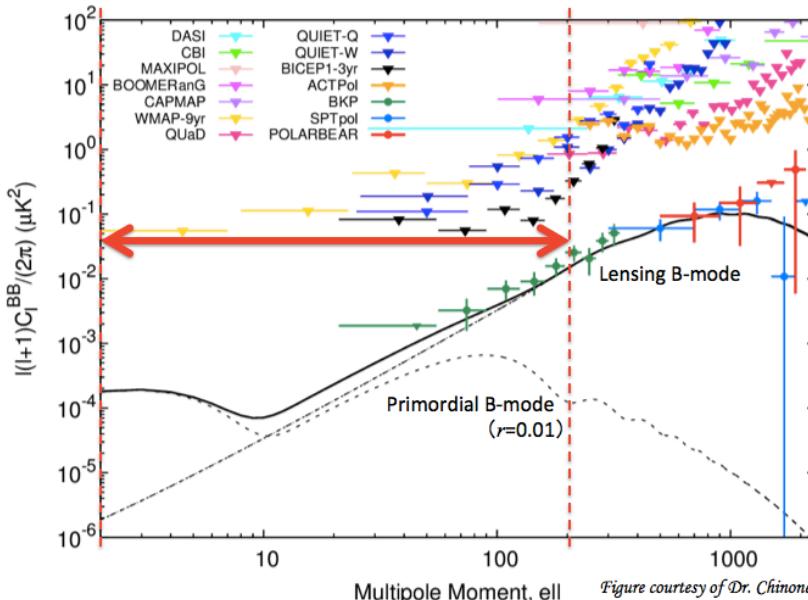
# What's the path forward to the future B-mode telescope design and some considerations?

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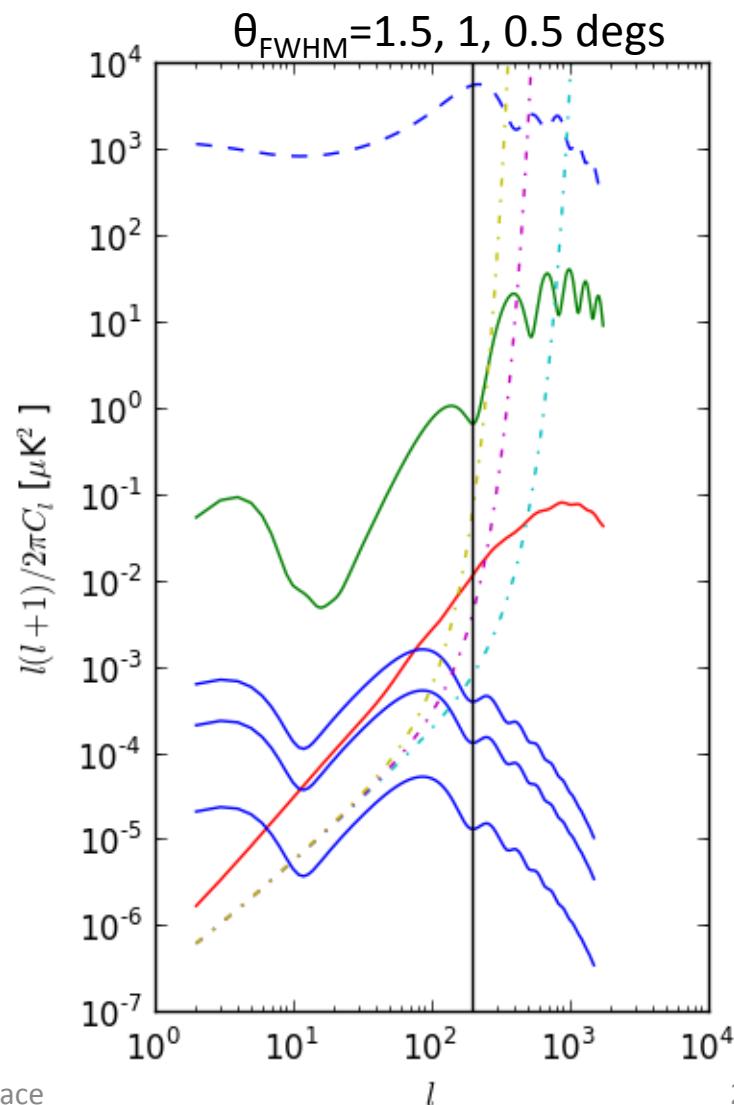


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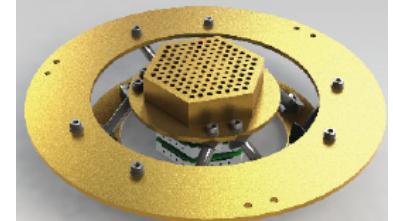
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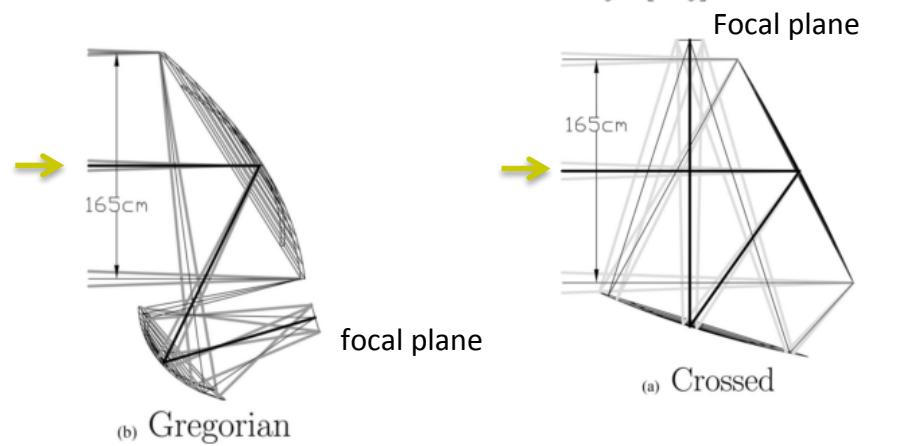
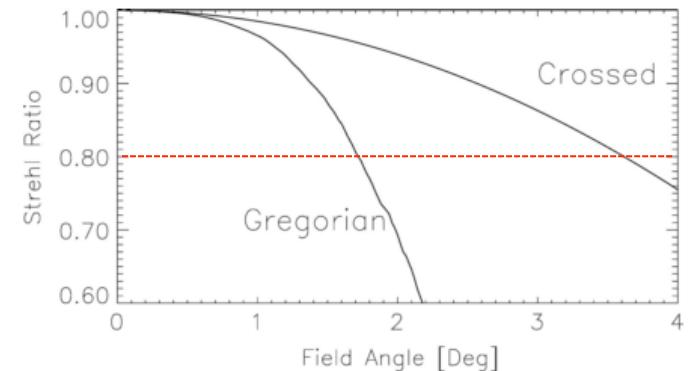
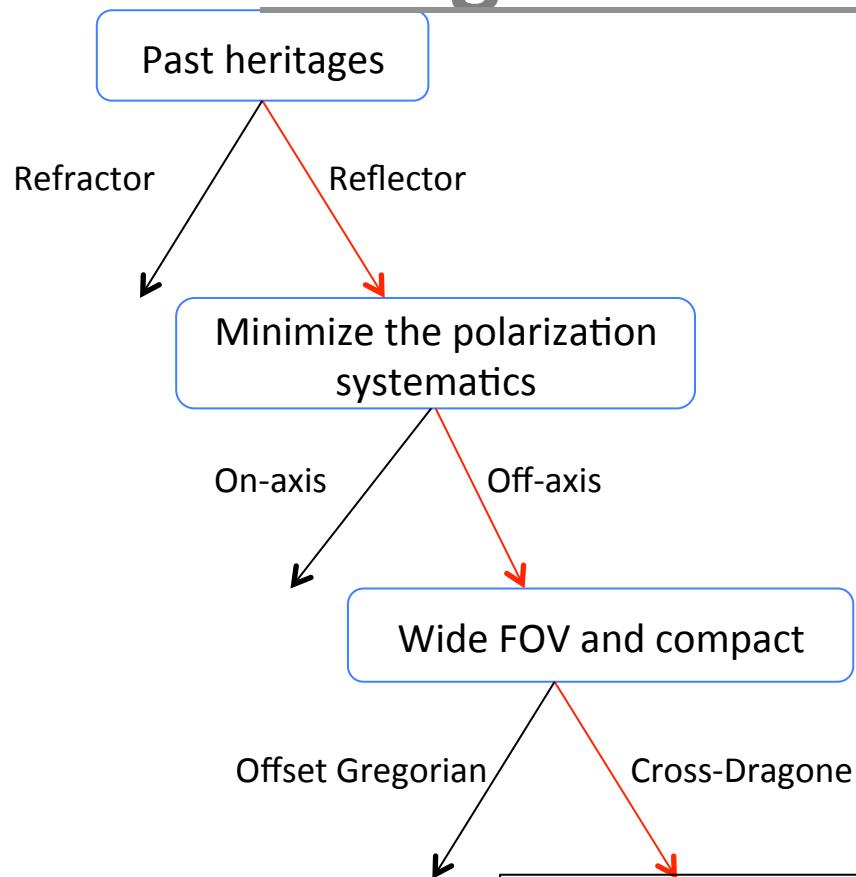
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# Design decision tree: example1

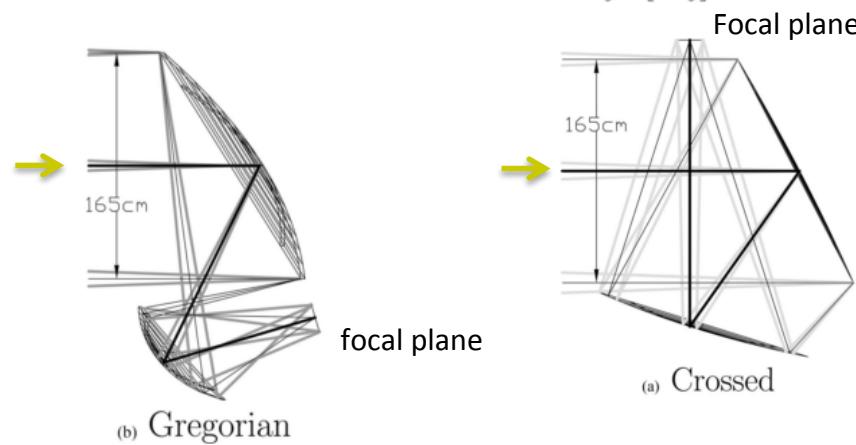
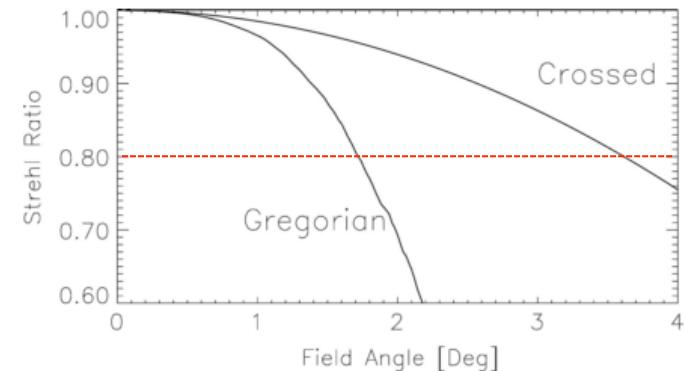
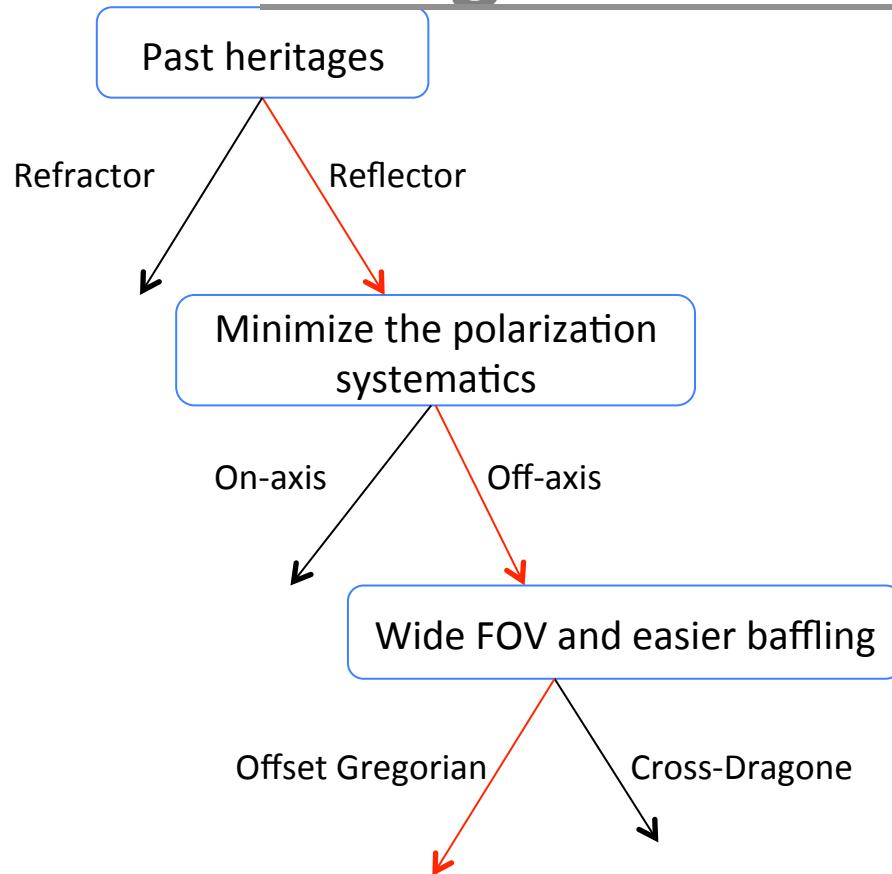


## Remaining challenges

1. Optical design
2. Cross-Dragone configuration is known to be susceptible to the stray light, and thus the optical design should include the baffle design. Verification by GRASP and beam map type measurements.
3. Make the optical element broadband
4. Thermal and structural design and fabrication feasibility study

B-mode from space

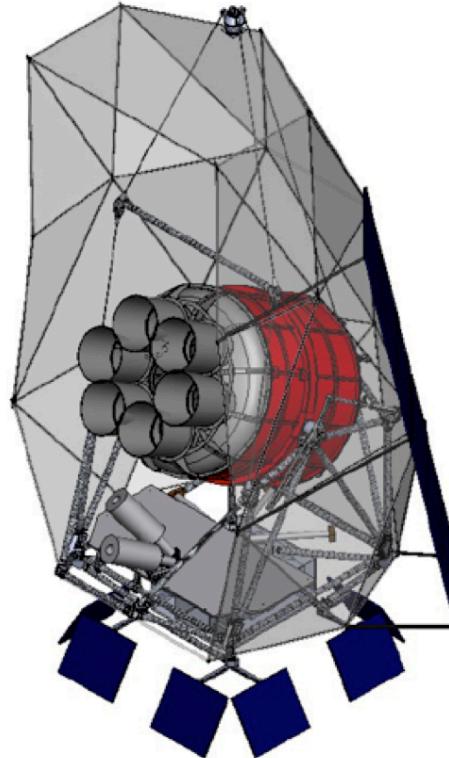
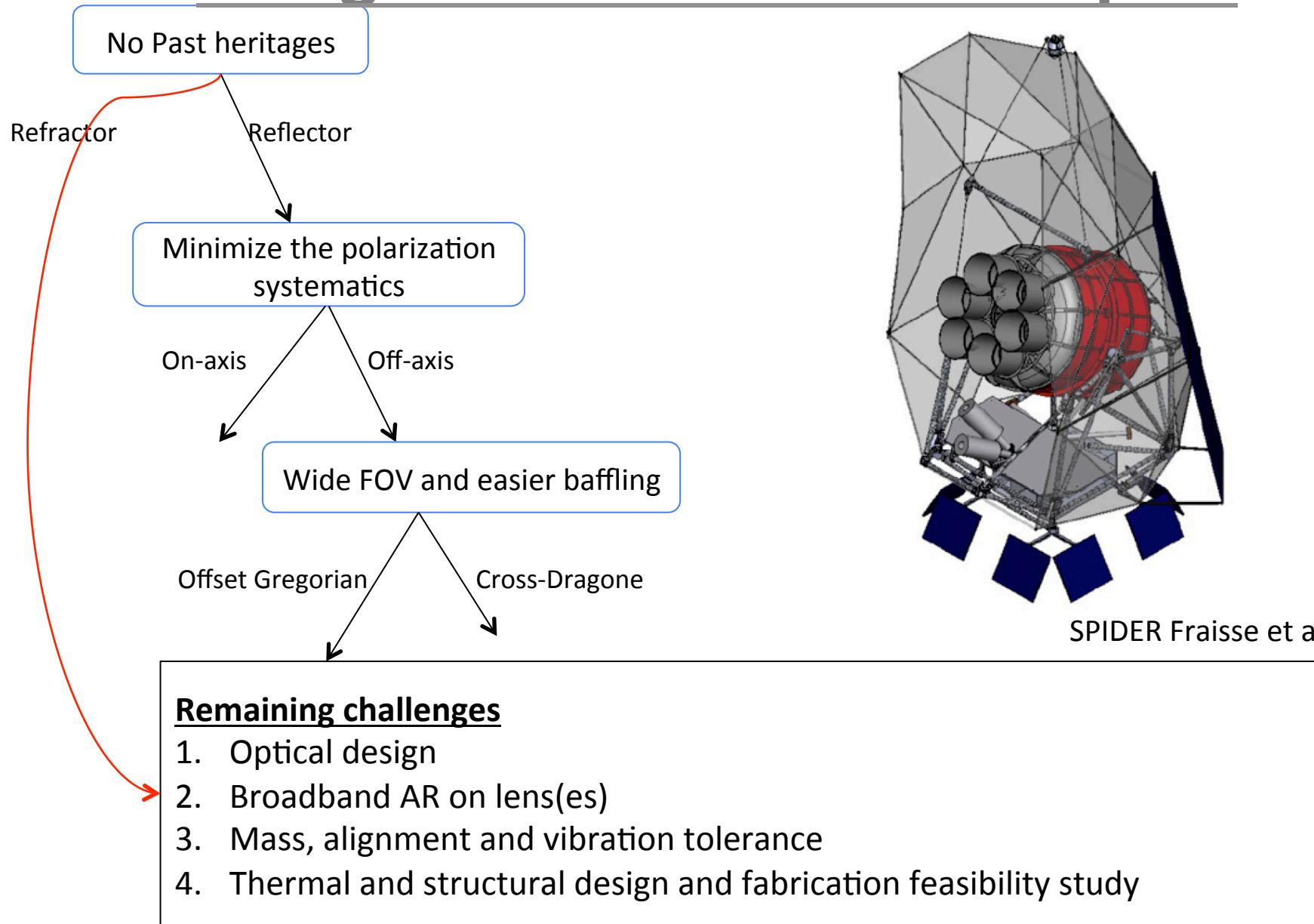
# Design decision tree: example2



## Remaining challenges

1. Optical design
2. Offset-Gregorian is known to have a non-telecentric prime focus and introduce the reimaging cold optics to achieve the wide telecentric FOV.
3. Broadband AR on lens(es) and assess the impact of a (probably) bigger envelop.
4. Maybe the HWP won't be the first element? Reflective metal-mesh HWP with even bigger envelop?

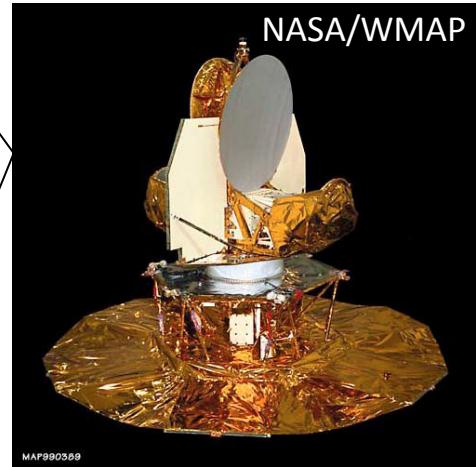
# Design decision tree: example3



SPIDER Fraisse et al. (2013)



# mm ~ THz space telescope



**Planck(ESA)** Obs. end  
Obs. Freq.: 24-857 GHz  
Aperture dia.: 1.5×1.9m  
Temp.: 45 K (passive cooling)  
Material: CFRP

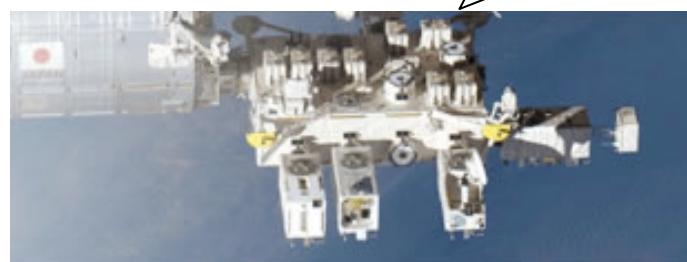
**WMAP (NASA)** Obs. end  
Obs. Freq.: 20-100 GHz  
Aperture dia.: 0.7m  
Temp.: 70 K (passive cooling)  
Material: CFRP (XN70)



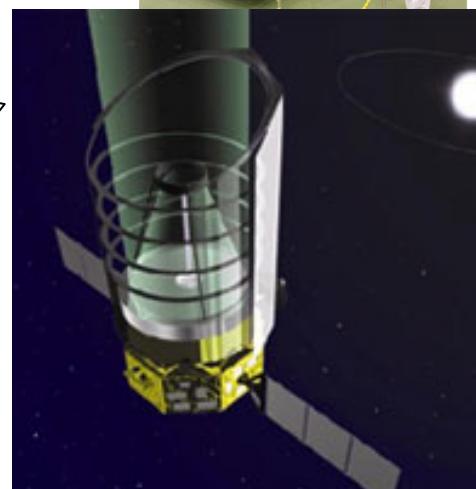
**AKARI (JAXA)** Obs. end  
Obs. Freq.: 1.7-180 $\mu$ m  
Aperture dia.: 0.7m  
Temp.: 6 K (Liquid  $^4$ He)  
Material: SiC

**SMILES(JAXA)** Obs. end  
Obs. Freq.: 625-650 GHz  
Aperture dia.: 40cmx20cm  
Temp.: Warm and 4K  
Material: aluminum

**Earthcare (JAXA)** in Prep.  
Obs. Freq.: 94GHz (W-band)  
Aperture dia.: 2.5 m  
Temp.: room  
Material: CFRP



**SPICA (JAXA)** Future sate.  
Obs. Freq.: IR  
Aperture dia.: >2m ?  
Temp.: 6 K ? (actively cooled)  
Material: C/SiC



**ISS** Ongoing  
B-mode from space  
1-2 years of exposure of CFRP mirror experiment at ISS

# Material choices

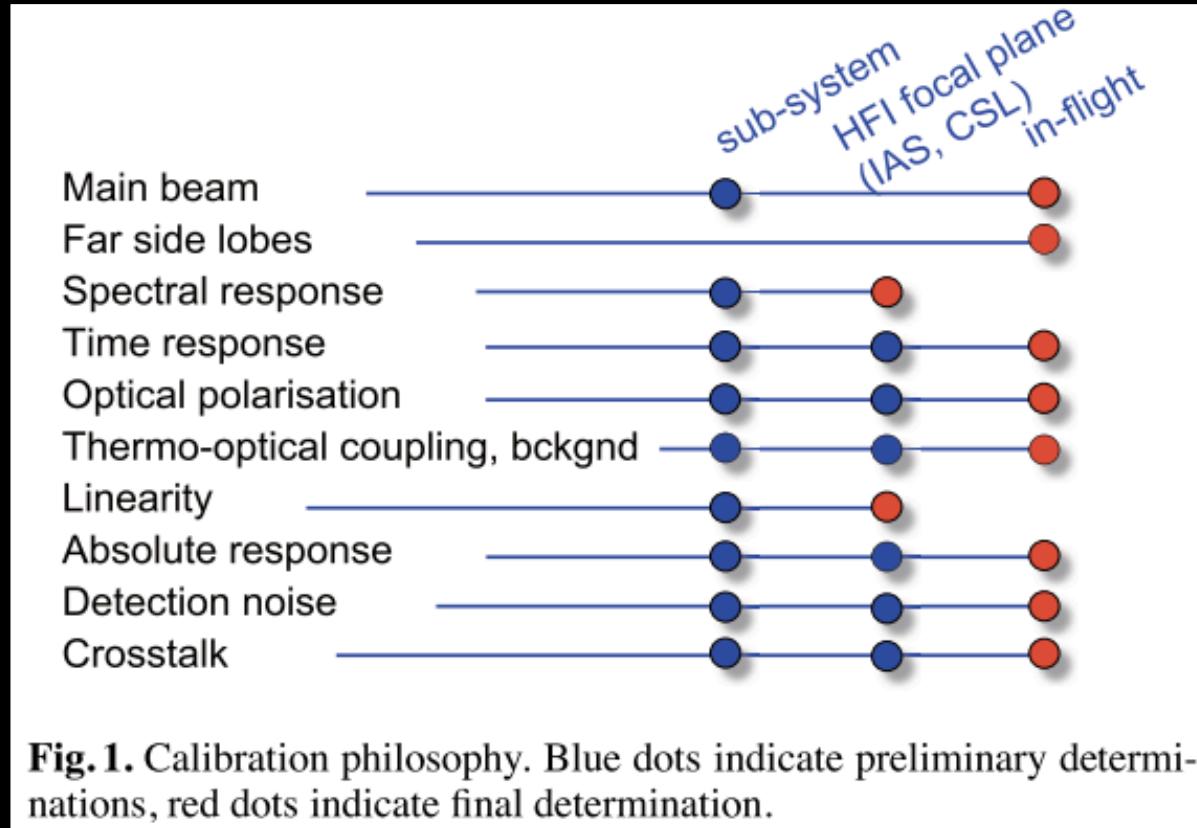
- Mirror
  - The material choice of the mirror body will be the interesting parameters. The choices may be
    - Aluminum
    - CFRP
    - SiC
    - C/SiC
    - Zero-expansion ceramic type material
- Lens
  - The choice would be tightly coupled to the AR coating methods
    - UHMWPE/HDPE
    - Si
    - Alumina
    - Meta-material-based lens
- Absorber choice
  - The current generation experiment is fan of coating with a cold black body material in order to absorb the stray light to mitigate the instrumentally induced polarization.
  - The aperture is one critical place on its choice.
  - Inner shell of the optics envelop
  - Mass is always an important metric for space mission

FOM:

- Mass
- Thermal expansion
- AR

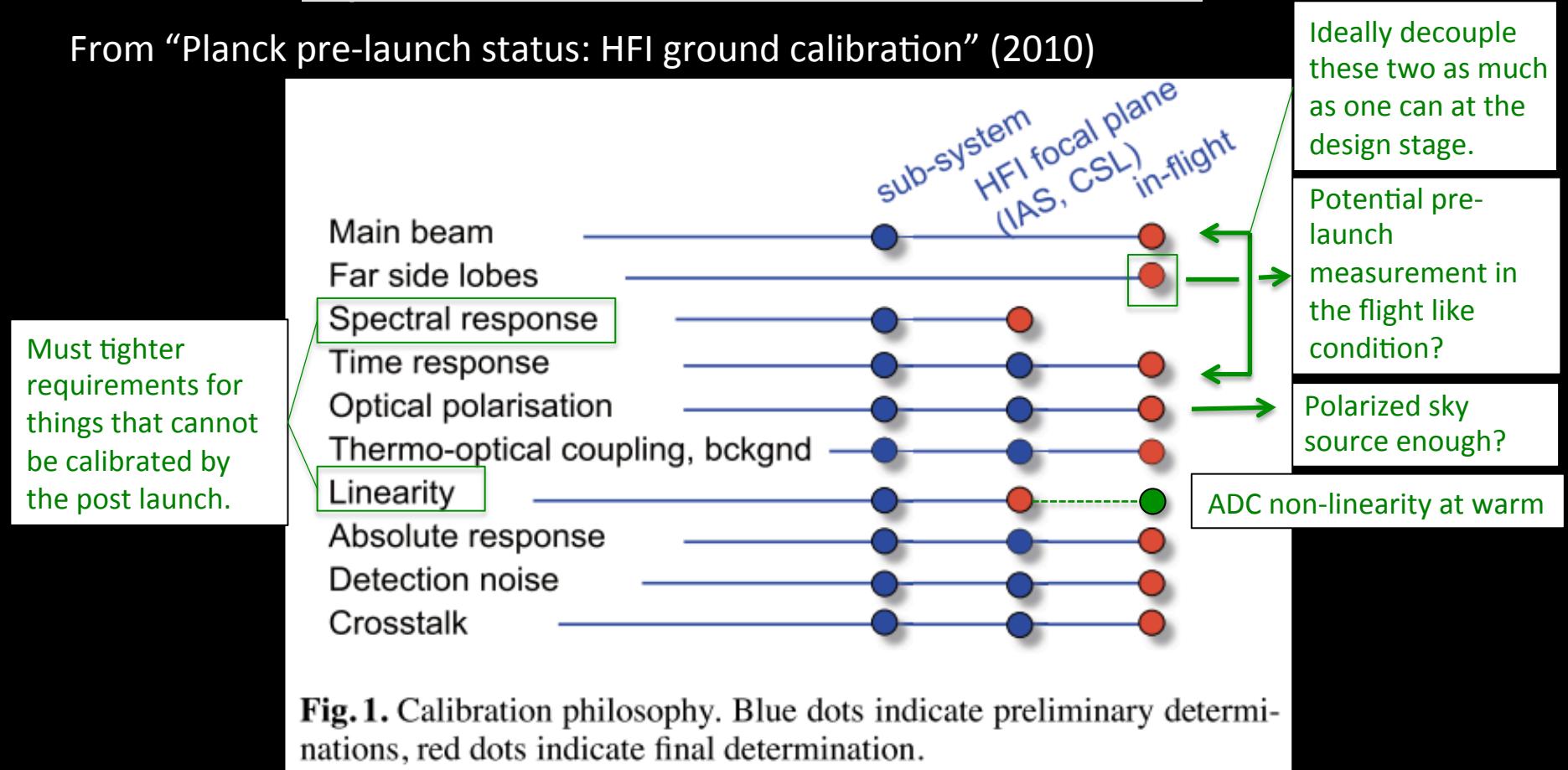
# Systematics and Calibration

From “Planck pre-launch status: HFI ground calibration” (2010)



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From “Planck pre-launch status: HFI ground calibration” (2010)



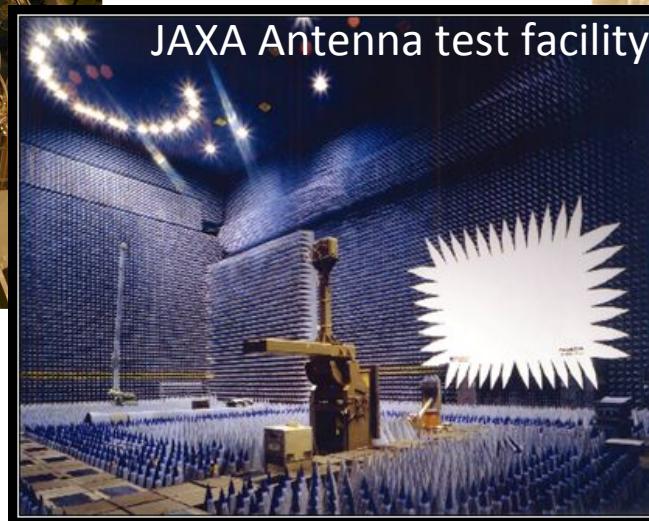
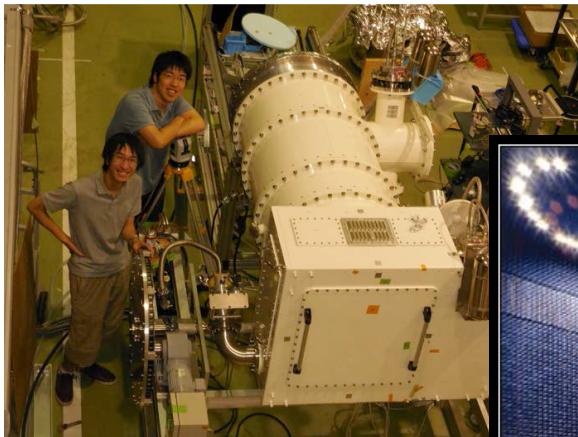
**Fig. 1.** Calibration philosophy. Blue dots indicate preliminary determinations, red dots indicate final determination.

Things that are not listed and could have listed are

- **Cosmic ray susceptibility of the system including the detector**
- Anything else?

# Testing and integrations

POLARBEAR2 integration is ongoing at KEK with sub-K cryogenic system and UC Berkeley TES bolometers.



More comes from the optics calibration session tomorrow.

How much do we rely on the simulation? Computational time is non-negligible with GRASP type software.

December 15, 2015



JAXA 13-m diameter space chamber

Astro-H test is done here.



JAXA 6-m diameter space chamber



JAXA 1-m diameter space chamber